

# Impulsive acceleration of strongly magnetized relativistic flows

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## ABSTRACT

The strong variability of magnetic central engines of active galactic nuclei (AGNs) and gamma-ray bursts (GRBs) may result in highly intermittent strongly magnetized relativistic outflows. We find a new magnetic acceleration mechanism for such impulsive flows that can be much more effective than the acceleration of steady-state flows. This impulsive acceleration results in kinetic-energy-dominated flows that are conducive to efficient dissipation at internal magnetohydrodynamic shocks on astrophysically relevant distances from the central source. For a spherical flow, a discrete shell ejected from the source over a time  $t_0$  with Lorentz factor  $\Gamma \sim 1$  and initial magnetization  $\sigma_0 = B_0^2/4\pi\rho_0c^2 \gg 1$  quickly reaches a typical Lorentz factor  $\Gamma \sim \sigma_0^{1/3}$  and magnetization  $\sigma \sim \sigma_0^{2/3}$  at the distance  $R_0 \approx ct_0$ . At this point, the magnetized shell of width  $\Delta \sim R_0$  in the laboratory frame loses causal contact with the source and continues to accelerate by spreading significantly in its own rest frame. The expansion is driven by the magnetic pressure gradient and leads to relativistic relative velocities between the front and back of the shell. While the expansion is roughly symmetric in the centre of the momentum frame, in the laboratory frame, most of the energy and momentum remains in a region (or shell) of width  $\Delta \sim R_0$  at the head of the flow. This acceleration proceeds as  $\Gamma \sim (\sigma_0 R/R_0)^{1/3}$  and  $\sigma \sim \sigma_0^{2/3} (R/R_0)^{-1/3}$  until reaching a coasting radius  $R_c \sim R_0 \sigma_0^2$ , where the kinetic energy becomes dominant:  $\Gamma \sim \sigma_0$  and  $\sigma \sim 1$  at  $R_c$ . The shell then starts coasting and spreading (radially), its width growing as  $\Delta \sim R_0 (R/R_c)$ , causing its magnetization to drop as  $\sigma \sim R_c/R$  at  $R > R_c$ . Given the typical variability time-scales of AGNs and GRBs, the magnetic acceleration in these sources is a combination of the quasi-steady-state collimation acceleration close to the source and the impulsive (conical or locally quasi-spherical) acceleration farther out. The interaction with the external medium, which can significantly affect the dynamics, is briefly addressed in the discussion.

**Key words:** MHD – relativistic processes – methods: analytical – gamma-ray burst: general – ISM: jets and outflows – galaxies: jets.

## 1 INTRODUCTION

The first question raised by the discovery of astrophysical jets is how they are powered, collimated and accelerated. Most of them – jets from young stars, active galactic nuclei (AGNs), Galactic X-ray binaries and gamma-ray bursts (GRBs) – are associated with disc accretion,<sup>1</sup> and this suggests that accretion discs are essential for

jet production. The astrophysical jets seem to be highly supersonic as many of their features are nicely explained by internal shocks. In the laboratory, highly collimated supersonic jets are normally produced when a high pressure (and temperature) gas escapes from a chamber via a finely designed nozzle. However, it seems highly unlikely that such refined ‘devices’ are formed naturally in astrophysical systems. They would require cold and dense gas to form the walls of the chamber with a massive compact object in the centre (Blandford & Rees 1974), but such configurations are highly unstable (Norman et al. 1981; Smith et al. 1983). This has led to the idea that the collimation of astrophysical jets may have a completely different mechanism involving a strong magnetic field. Although this magnetic field still needs to be confined within a channel, the conditions on its geometry are less restrictive. If this field is anchored to a rotating object, such as an accretion disc, then it naturally

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<sup>1</sup> The only exceptions are the jets of pulsar wind nebulae as there are no indications of accretion discs around their pulsars. These jets are most likely not produced directly by the pulsars, but from downstream of the termination shock of pulsar winds (Lyubarsky 2002; Komissarov & Lyubarsky 2004).

develops an azimuthal component. The hoop stress associated with this magnetic field component creates additional collimation of the flow within the channel. Moreover, this leads to a magnetic torque being applied to the rotating object and thus a natural way of powering outflows by tapping the rotational energy of the central object.

In order to produce a relativistic flow this way, the magnetic energy per particle must exceed its rest energy. Thus, the jet plasma must be highly rarefied. Such rarefied plasma is naturally produced only in the magnetospheres of black holes and neutron stars. Moreover, the strong magnetic field shields these magnetospheres and prevents them from being contaminated by the much denser surrounding plasma. In contrast, young stars can eject a lot of mass from their surface and this seems to explain why their jets are not relativistic. Magnetospheres of accretion discs are likely to be heavily mass-loaded and are not able to produce relativistic jets for the same reason.

It has to be stressed that magnetic flows must still be collimated externally until they become superfast magnetosonic. The magnetic hoop stress can result in self-collimation of the inner core but cannot prevent sideways expansion of the outer sheath. However, when the flow becomes superfast magnetosonic, the speed of this lateral expansion becomes smaller than the flow speed along the jet direction, and the jet remains collimated. For non-relativistic jets, the condition of passing through the fast-magnetosonic surface also implies almost completed acceleration of the flow (50 per cent conversion of magnetic energy into kinetic energy). In contrast, the relativistic jets still remain Poynting-flux-dominated at this point and the acceleration process may continue well into the superfast-magnetosonic regime.

The issue of the efficiency of energy conversion (from magnetic to kinetic form) is related to the issue of subsequent energy dissipation, which is required in order to explain the observed electromagnetic emission from both the jets and the structures they create when they collide with the external medium. Traditionally, one of the most favourite channels of dissipating the energy of supersonic flows has been the formation of shock waves. However, in the case of relativistic flows, this mechanism can be much less efficient, if the flow is Poynting-flux-dominated. First of all, it is the kinetic energy of the flow that is dissipated,<sup>2</sup> and if only a small fraction of the total energy is in the kinetic form, then this severely limits the efficiency of dissipation. Secondly, the compression ratio and hence the fraction of kinetic energy that dissipates also decreases with increasing magnetization. Thus, in order to dissipate a significant fraction of the available energy, the flow should not only become superfast magnetosonic, but it should also become dominated by kinetic energy before it is shocked (Leismann et al. 2005; Mimica, Giannios & Aloy 2009; Mimica & Aloy 2010).

The magnetic acceleration of relativistic flows has been the subject of theoretical research for decades. The main focus of this research has been on the models of steady-state axisymmetric dissipation-free flows (the ‘standard model’). The main reason behind this is simplicity. Only in this case was there a hope of building a rigorous theory. However, even this idealized model is rather complex, and solutions could be found only if an additional symmetry was introduced, such as self-similarity or another simplifying condition (e.g. Begelman & Li 1992; Vlahakis & Königl 2003; Beskin &

Nokhrina 2006). More recently the problem was approached using numerical methods (Komissarov et al. 2007, 2009a).

There are a number of problems with the standard model, which are most severe in the case of a spherical wind. In this case, the theory predicts an asymptotic Lorentz factor of  $\Gamma \sim \sigma_0^{1/3}$ , where  $\sigma_0 = B_0^2/4\pi\rho_0c^2 \gg 1$  is the initial magnetization parameter, which determines the maximum possible Lorentz factor corresponding to a total conversion of the Poynting flux into the bulk motion kinetic energy in a steady-state flow (e.g. Goldreich & Julian 1970). This is in conflict with the observations of many astrophysical sources. In particular, the high observed values of  $\Gamma$  in many sources would require an extremely large initial magnetization  $\sigma_0$  that would in turn imply a very high asymptotic magnetization,  $\sigma \sim \sigma_0^{2/3} \gg 1$ , making it impossible to achieve efficient shock dissipation within the outflow.

A potential way to overcome this problem is by resorting to collimated outflows. This can increase the asymptotic value of  $\Gamma$  and reduce that of  $\sigma$  by up to a factor of  $\sim \theta_{\text{jet}}^{-2/3}$ , where  $\theta_{\text{jet}}$  is the asymptotic half-opening angle of the jet. The collimation has to be strong enough to preserve causal connectivity across the flow (in the lateral direction). The faster the flow and the higher its fast-magnetosonic Mach number becomes, the smaller its opening angle should be. By the time one half of the Poynting flux is converted into kinetic energy ( $\sigma \sim 1$ ), the jet half-opening angle  $\theta_{\text{jet}}$  should not exceed  $\theta_{\text{max}} = 1/\Gamma$ , where  $\Gamma \sim \sigma_0$  is the jet Lorentz factor at that time. Observations of AGN jets do indeed show that  $\theta_{\text{jet}} < 1/\Gamma$  (Pushkarev et al. 2009). However, for GRB jets with  $\Gamma \simeq 400$  (or  $10^2 \lesssim \Gamma \lesssim 10^{3.5}$ ), this constraint gives  $\theta_{\text{max}} \simeq 0.14$  (or  $0.018 \lesssim \theta_{\text{max}} \lesssim 0.57$ ), which is much smaller compared to generally accepted values of the half-opening angle,  $2^\circ \lesssim \theta_{\text{jet}} \lesssim 30^\circ$  (Frail, Waxman & Kulkarni 2000; Panaitescu & Kumar 2001).

In addition, the standard theory of GRB afterglow emission can explain the jet break in their light curves only if  $\theta_{\text{jet}}\Gamma \gg 1$  (Rhoads 1999; Sari, Piran & Halpern 1999). Although the *Swift* observations show that clear jet breaks are not as common as we used to think (e.g. Liang et al. 2008), this might be at least partly due to observational selection effects (*Swift* GRBs are dimmer on average as *Swift* is more sensitive than previous missions) and there are still some clear cases for jet breaks in the *Swift* era. Finally, late-time radio afterglow observations, when the flow becomes subrelativistic, provide fairly robust (no longer susceptible to strong relativistic beaming) lower limits (e.g. Eichler & Waxman 2005) on the true energy that remains in the afterglow blast wave at that time, of a few to several times  $10^{51}$  erg (Berger, Kulkarni & Frail 2004; Frail et al. 2005). Such a large true energy, together with the inferred energy per solid angle in the prompt gamma-ray emission and in the afterglow shock at early times, implies that the initial jet half-opening angle cannot be too small (typically not much less than a few degrees).

It turns out that a transition from laterally confined to ballistic flow is accompanied by a relatively short phase of acceleration of a different kind (Komissarov, Vlahakis & Königl 2010; Tchekhovskoy, Narayan & McKinney 2009). Such a transition may occur in the collapsar model at the stellar surface. A sudden loss of lateral pressure support causes a sideways expansion of the jet. If the jet is highly relativistic at the stellar surface, then the corresponding increase in the jet opening angle is negligible. However, a rarefaction wave propagates into the jet and brings it out of lateral balance. The magnetic pressure force accelerates the flow in the lateral direction, which results in a significant increase in the jet Lorentz factor, particularly in the outer layers of the jet. This may alleviate the  $\theta_{\text{jet}}\Gamma \simeq 1$  problem of the magnetic model. However, as soon as the rarefaction crosses the jet, it is well in the ballistic regime and

<sup>2</sup> This applies to fast-magnetosonic shocks. At a slow-magnetosonic shock, the magnetic energy dissipates as well and the kinetic energy can actually increase. However, slow shocks are much less robust and harder to generate compared to the fast ones.

the acceleration is over.<sup>3</sup> Moreover, it does not ensure full conversion of electromagnetic energy to kinetic energy. If this happens a bit too soon then the jet remains Poynting-flux-dominated. Even under the best of circumstances the resultant jet magnetization is still close to  $\sigma \simeq 1$ , which is too high for effective shock dissipation (Leismann et al. 2005; Mimica et al. 2009; Mimica & Aloy 2010).

Given the problems with this basic case, other ideas have been put forward. The most radical idea is to assume that relativistic astrophysical jets do not become kinetic-energy-dominated, but remain Poynting-flux-dominated on all scales, and that the observed emission comes not from shocks, but from magnetic dissipation sites (Blandford 2002; Lyutikov 2006). In the context of this work, this may potentially serve as an alternative to internal shocks in cases where for some reason the magnetization remains high at large distances from the source. Others propose various ways of increasing the efficiency of magnetic acceleration compared to the basic model, for example, via allowing non-axisymmetric instabilities and randomization of magnetic field (Heinz & Begelman 2000). In fact, the magnetic dissipation may also help the transition from Poynting-flux-dominated to kinetic-energy-dominated states (Drenkhahn 2002; Drenkhahn & Spruit 2002).

In this work, we focus on the acceleration of an impulsive (strongly time-dependent) highly magnetized relativistic outflow, which has received relatively little attention so far. Contopoulos (1995) was first to consider the non-relativistic case of impulsive magnetic acceleration and dubbed it an ‘astrophysical plasma gun’. The relativistic version presents a number of qualitatively different properties. In Section 2, we present a detailed study of a simplified test case featuring a cold and initially highly magnetized ( $\sigma_0 \gg 1$ ) one-dimensional finite shell (of initial width  $l_0$ ) initially at rest (at  $t = 0$ ), whose back end leans against a ‘wall’ and with vacuum in front of it. The initial evolution (Section 2.1 and Appendix A) is described by a self-similar rarefaction wave travelling towards the wall and accelerating the Poynting-flux-dominated flow away from the wall. At the end of this phase, at time  $t_0 \approx l_0/c$ , when the rarefaction wave reaches the wall, the mean Lorentz factor of the flow is  $\langle \Gamma \rangle \sim \sigma_0^{1/3}$ . Soon after  $t_0$  the shell separates from the wall and moves away from it (Section 2.2). The shell continues to accelerate and keeps an almost constant width of  $\sim 2l_0$ . Using both numerical (Section 2.3) and analytical (Sections 2.2 and 3.2, and Appendixes C3 and F2) methods, we find that during the second phase, the mean Lorentz factor grows as  $\langle \Gamma \rangle \sim (\sigma_0 t/t_0)^{1/3} \propto t^{1/3}$ . This phase ends at time  $t_c = t_0 \sigma_0^2$ , when the acceleration slows down and the shell starts coasting. At this point  $\langle \Gamma \rangle \sim \sigma_0$  and  $\sigma \sim 1$ . In Section 3, we present crude but simple derivations of the main results of Section 2 that allow us to understand the underlying physics and show that the results are robust – not very sensitive to the exact initial configuration. The analysis of the coasting phase (Section 3.3) shows that at  $t > t_c$ , the shell width increases as  $\Delta \sim 2l_0 t/t_c \propto t$ , while its magnetization decreases as  $\sigma \sim t_c/t \propto t^{-1}$ , resulting in a kinetic-energy-dominated flow.

In Section 4, we address the apparent paradox of self-acceleration – how can the shell keep accelerating after it separates from the wall? We analyse a variation of our simple test case in which the wall is removed when the rarefaction wave reaches it (at  $t_0$ ). At subsequent times, there are no external forces on the system, implying that the centre of momentum (CM) velocity or Lorentz

factor ( $\Gamma_{\text{CM}}$ ) remains constant and there is no global acceleration at  $t > t_0$  in this strict sense. Nevertheless, even though we find that  $\Gamma_{\text{CM}} \sim \sigma_0^{1/2}$  remains constant, the more relevant astrophysical quantity is the mean value of  $\Gamma$  weighted over the energy in the laboratory frame,  $\langle \Gamma \rangle_E$ , and it indeed increases as  $\langle \Gamma \rangle_E \sim (\sigma_0 t/t_0)^{1/3}$  at  $t_0 < t < t_c$ . In Section 5, we discuss the connection between our test case and relativistic astrophysical flows, and study the possible implications of our impulsive acceleration mechanism for the dynamics of GRB and AGN jets. We also briefly address the interaction of the magnetized flow with the external medium for GRBs. Our main results and conclusions are presented in Section 6.

Soon after the first version of our paper appeared on the electronic archive (<http://arxiv.org/archive/astro-ph/>), an independent study of impulsive magnetic acceleration was published there as well (Lyutikov 2010a,b; Lyutikov & Lister 2010), indicating growing interest in this mechanism. Where the covered topics overlap, the results of both studies agree very well. As to the differences, their study focuses on the initial phase of fast acceleration (at  $t < t_0$ ) and shock formation (when instead of pure vacuum the shell expands into a rarefied plasma), whereas the main subject of our paper is the operation of the impulsive acceleration mechanism after the shell separates from the ‘wall’ (at  $t > t_0$ ).

## 2 TEST CASE: EXPANSION OF A MAGNETIZED SHELL INTO VACUUM

A good way of demonstrating the basic dynamics of the acceleration of a highly magnetized impulsive flow is to start with a simple example that can be analysed analytically or using simple one-dimensional simulations. To this aim we consider for our initial conditions a uniform shell of width  $l_0$  with high initial magnetization,  $\sigma_0 = B_0^2/4\pi\rho_0 c^2 \gg 1$ , where  $B_0$  is the initial magnetic field and  $\rho_0$  is the initial rest-mass density. We choose Cartesian coordinates in which the plane of the shell is perpendicular to the  $x$ -axis and the magnetic field is aligned with the  $y$ -axis. The right-hand boundary of the shell is at  $x = 0$  and the left-hand one is at  $x = -l_0$ . To the left-hand side of the shell is a solid conducting wall and to the right-hand side is a vacuum.

### 2.1 Self-similar rarefaction phase

At time  $t = 0$ , we allow the shell to expand into vacuum. This is a well-known problem that describes a simple rarefaction wave propagating into the shell towards the wall. The self-similar simple wave solution to the general case with non-vanishing thermal pressure is described in Appendix A. Here we focus only on the cold limit (with no thermal pressure; the equations describing this case reduce to those of the pure gas case with an adiabatic index  $\gamma = 2$ ).

Using units where  $c = 1$ , the local wave speed is

$$\lambda = \frac{v - c_{\text{ms}}}{1 - v c_{\text{ms}}}, \quad (1)$$

where  $c_{\text{ms}}$  is the fast-magnetosonic speed as measured in the fluid frame.<sup>4</sup> In our (cold) limit

$$c_{\text{ms}}^2 = \frac{\sigma}{1 + \sigma}, \quad (2)$$

where

$$\sigma = \frac{B'^2}{4\pi\rho} = \frac{(B/\Gamma)^2}{4\pi\rho}$$

<sup>3</sup> This is in contrast with the highly robust mechanism of thermal acceleration, where for an adiabatic index of  $\gamma = 4/3$ , the jet Lorentz factor grows linearly with the jet radius,  $\Gamma \propto R$ , even in the ballistic regime.

<sup>4</sup> This is simply the Lorentz transformation of a velocity component parallel to the relative velocity of two inertial frames.

is the local magnetization parameter, while  $B' = B/\Gamma$  and  $\rho$  are the magnetic field and the rest-mass density, respectively, as measured in the fluid rest frame. The equations of one-dimensional motion yield

$$\frac{B'}{\rho} = \frac{B}{\Gamma\rho} = \text{constant} \quad (3)$$

(see Appendix A) and thus

$$\sigma = \sigma_0 \frac{\rho}{\rho_0}. \quad (4)$$

The backward characteristics of the simple wave (where the wave moves in the direction opposite to that of the flow) are straight lines described by

$$\xi = \lambda = \frac{v - c_{\text{ms}}}{1 - v c_{\text{ms}}}, \quad (5)$$

where  $\xi = x/t$  is the self-similar variable. Integration of the self-similar flow equation gives [see equation (A26) for  $\gamma = 2$  or equations (A29) and (A24) for  $a_0 = 0$ ]

$$\frac{1+v}{1-v} \left( \frac{1+c_{\text{ms}}}{1-c_{\text{ms}}} \right)^2 = \mathcal{J}_+, \quad (6)$$

where

$$\mathcal{J}_+ = \left( \frac{1+c_{\text{ms},0}}{1-c_{\text{ms},0}} \right)^2 = \left( \sqrt{\sigma_0} + \sqrt{\sigma_0 + 1} \right)^4 \approx 16\sigma_0^2,$$

where the last equality holds for  $\sigma_0 \gg 1$ . This equation, in combination with equations (2) and (4), allows to find  $\rho = \rho(v)$  and then equation (3) gives  $B = B(v)$ . Finally, equation (5) allows us to find the dependence of all flow variables on  $\xi$ .

Fig. 1 shows the self-similar solution for  $\sigma_0 = 30$ , in units where  $\rho_0 = l_0 = c = 1$ , at time  $t = 1$  (when the left-hand front of the rarefaction wave is about to reach the wall). One can see that both the left- and the right-hand fronts of the wave propagate at very close to the speed of light. The magnetic field and the total energy density distributions in the expanding shell are almost uniform (except for the thin boundary layers). This is expected as the plasma inertia is very low and the electromagnetic part of the solution must be close to the corresponding solution of the Maxwell equations. Near the right-hand front, the distributions of most flow parameters exhibit large gradients. In the plots of the Lorentz factor and total kinetic energy density, we see narrow spikes. The maximum value of the Lorentz factor can be found from equation (6) by setting  $c_{\text{ms}} = 0$ . For  $\sigma_0 \gg 1$ , we find

$$\Gamma_{\text{max}} \approx 2\sigma_0. \quad (7)$$

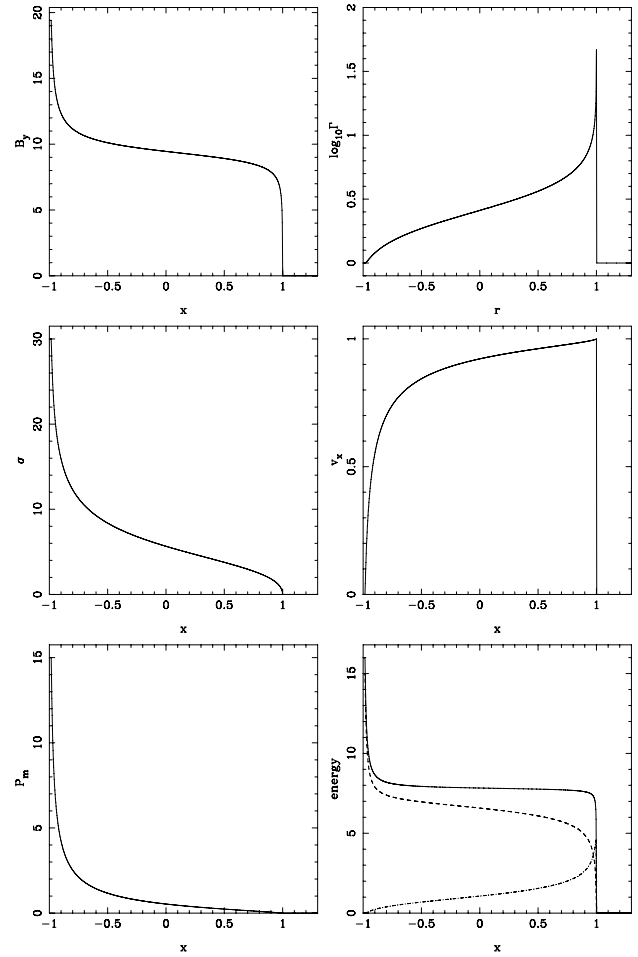
This is already a very high speed. However, only a very small fraction of the flow energy is associated with this spike and the mean Lorentz factor is much lower. Fig. 1 suggests that the mean Lorentz factor must be close to that of the sonic point,  $\xi = 0$ , for which equation (6) gives (for  $\sigma_0 \gg 1$ ):

$$\Gamma(\xi = 0) \approx \left( \frac{\sigma_0}{2} \right)^{1/3}. \quad (8)$$

More sophisticated averaging procedures (such as the weighted averages over the energy or rest mass) described in Appendix B give values only slightly higher (see the right-hand panel of Fig. B1) and show that

$$\langle \Gamma \rangle \simeq \sigma_0^{1/3} \quad (9)$$

is a very good estimate.



**Figure 1.** The self-similar rarefaction wave solution at  $t = 1$ , using units of  $l_0 = 1$ ,  $\rho_0 = 1$  and  $c = 1$ . The initial conditions are a uniform state with parameters  $\sigma_0 = 30$  and  $v_0 = 0$  at  $-1 < x < 0$  and vacuum for  $x > 0$ . Shown are the magnetic field  $B_y$  (top left-hand panel), the Lorentz factor  $\Gamma$  (as measured in the wall frame; top right-hand panel), the local magnetization parameter,  $\sigma = (B')^2/4\pi\rho$  (middle left-hand panel), the flow velocity  $v_x$  (middle right-hand panel), the magnetic pressure  $p_m = (B')^2/8\pi$  (bottom left-hand panel) and the density of total energy (solid line), magnetic energy (dashed line) and kinetic energy (dot-dashed line) as measured in the wall frame (bottom right-hand panel).

## 2.2 Evolution after separation from the wall

At the time  $t = t_0 = l_0/c_{\text{ms}}(v = 0) \approx l_0$  (where we still use units of  $c = 1$ ), the left-hand front of the rarefaction wave reaches the wall and then the evolution of the shell changes. A secondary rarefaction wave is launched from the wall and propagates to the right-hand side, trying to catch up with right-hand front of the original wave. However, both fronts propagate with speeds very close to the speed of light and the spatial separation between them changes only very slowly – to the first approximation, it is  $\approx 2l_0$ . At  $t < t_0$ , the original rarefaction wave does not ‘know’ about the existence of the wall in the sense that it behaves according to the self-similar solution for a semi-infinite shell.<sup>5</sup> At  $t > t_0$ , however, this is true only ahead of

<sup>5</sup> It does ‘know’ about the wall in the sense that if instead of a wall at  $x = -l_0$  there would be vacuum at  $x = -l_0$  then the wave would be affected at  $t > t_0/2$ , and the front half of the shell would behave as in our original setup with a virtual ‘wall’ at  $x = -l_0/2$  (while the other half would behave as its mirror image with respect to this virtual ‘wall’).

the reflected rarefaction wave, at  $x > x_*(t)$  or  $\xi > \xi_*(t) = x_*(t)/t$ , where  $x_*(t)$  is the location of the front of the secondary rarefaction [ $x_*(t_0) = -l_0$ ]. At  $x > x_*(t)$ , the fluid continues to be accelerated by the pressure gradient created during the initial expansion.

At  $x < x_*(t)$ , however, inside the secondary wave, the density and pressure drop very rapidly and the fluid is decelerated by the strong magnetic pressure gradient that develops just behind the head of this wave. Moreover, the total rest mass in this region is very small and one can describe the shell evolution as a separation from the wall. This is in contrast with the non-relativistic version of this problem considered by Contopoulos (1995), where there is no such separation, and the flow pressure and density peak at the wall.<sup>6</sup> The Lorentz factor and kinetic energy, as measured in the laboratory frame, drop strongly behind the front of this wave and only the part of the initial flow that is not yet affected by the right rarefaction wave significantly contributes to the total energetics (see Fig. 2). Therefore, the ‘typical’ or mean (as averaged over the energy in the laboratory frame) Lorentz factor of the shell should behave as the fluid Lorentz factor  $\Gamma(\xi_*)$  at the front of the right-hand rarefaction wave (or the back boundary of the shell).

In the fluid frame, the front of secondary rarefaction moves with the local magnetosonic speed. In the laboratory frame, this corresponds to

$$\beta_* \equiv \frac{dx_*}{dt} = \frac{v(\xi_*) + c_{ms}(\xi_*)}{1 + v(\xi_*)c_{ms}(\xi_*)}. \quad (10)$$

In the ultrarelativistic accelerating regime, where  $v \simeq 1$  and  $c_{ms} \simeq 1$  [where the latter requirement ensures that there is still plenty of magnetic energy to drive the acceleration:  $\langle \sigma \rangle \sim \sigma(\xi_*) \gg 1$ ], it is more convenient to work with the corresponding Lorentz factors,  $\Gamma = (1 - v^2)^{-1/2}$  and  $\Gamma_{ms} = (1 - c_{ms}^2)^{-1/2}$ , using the approximation

$$v \approx 1 - \frac{1}{2\Gamma^2}, \quad c_{ms} \approx 1 - \frac{1}{2\Gamma_{ms}^2}. \quad (11)$$

Substituting these into equations (5) and (6) yields

$$\Gamma_{ms}^2 \approx \frac{\sigma_0}{2\Gamma} \quad (12)$$

and

$$\xi \approx \frac{(\Gamma/\Gamma_{ms})^2 - 1}{(\Gamma/\Gamma_{ms})^2 + 1}. \quad (13)$$

Combining equation (12) with equation (13), we obtain

$$\Gamma^3 \approx \frac{\sigma_0}{2} \left( \frac{1 + \xi}{1 - \xi} \right). \quad (14)$$

The final step is to find  $\xi_* = \xi_*(t)$  and substitute the result in equation (14). In fact, in the ultrarelativistic regime, equation (10) yields

$$\beta_* \equiv \frac{dx_*}{dt} \approx 1 - \frac{1}{8\Gamma^2(\xi_*)\Gamma_{ms}^2(\xi_*)} \approx 1 - \frac{1}{4\sigma_0\Gamma(\xi_*)}. \quad (15)$$

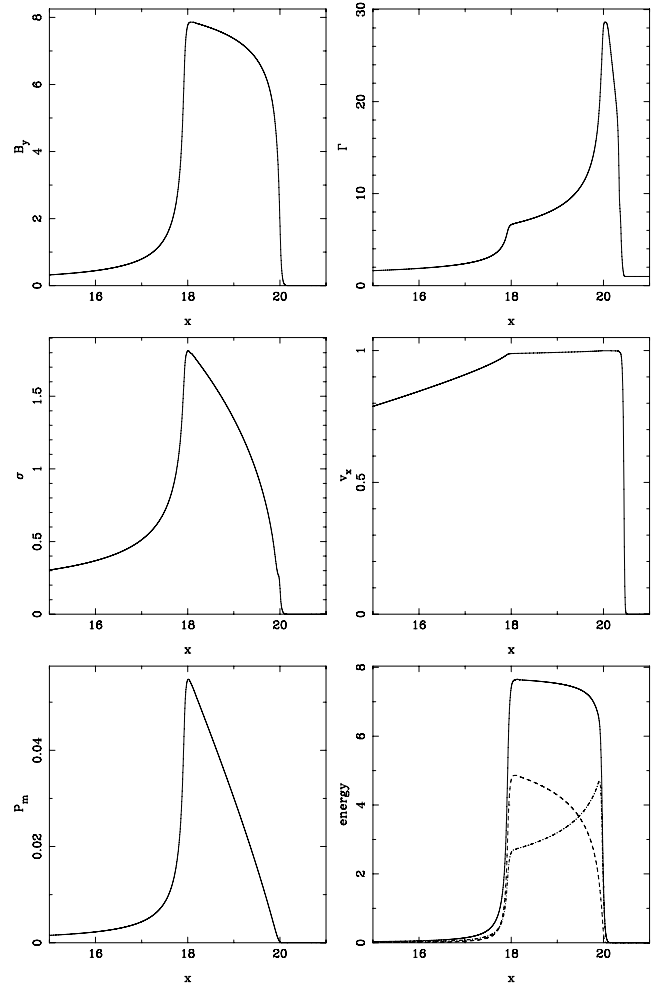
When  $\Gamma \ll \sigma_0$ , this can be simply approximated as  $\beta_* \approx dx_*/dt \approx 1$ , which gives

$$x_* \approx t - 2l_0, \quad \xi_* = \frac{x_*}{t} \approx 1 - \frac{2l_0}{t}, \quad (16)$$

(see Appendix C). Substituting this result in equation (14), we finally obtain

$$\Gamma(\xi_*) = \left( \frac{\sqrt{\mathcal{J}_+ t}}{8t_0} \right)^{1/3} \approx \left( \frac{\sigma_0 t}{2t_0} \right)^{1/3} \propto t^{1/3}. \quad (17)$$

<sup>6</sup> Thus, the relativistic dynamics of a magnetized shell is even closer to the ‘plasma gun’ action and also brings to mind the hypothetical ‘phasers’, all too familiar to the fans of the science-fiction series ‘Star Trek’.



**Figure 2.** Propagation of a highly magnetized cold shell of plasma. The plots describe the numerical solution at time  $t = 20$  for the same initial data as in Fig. 1 and use the same units. The top panels show the magnetic field  $B_y$  (top left-hand panel), the Lorentz factor  $\Gamma$  (as measured in the wall frame; top right-hand panel), the local magnetization parameter,  $\sigma = (B')^2/4\pi\rho$  (middle left-hand panel), the flow velocity  $v_x$  (middle right-hand panel), the magnetic pressure  $p_m = (B')^2/8\pi$  (bottom left-hand panel) and the density of total energy (solid line), magnetic energy (dashed line) and kinetic energy (dot-dashed line) as measured in the wall frame (bottom right-hand panel). The front of secondary rarefaction is located at  $x \simeq 18$ .

As a self-consistency check, we note that since  $\Gamma_* = (1 - \beta_*^2)^{-1/2} \gg 1$ ,  $\beta_* \approx 1 - 1/2\Gamma_*^2$ , equations (15) and (17) imply

$$\beta_* \approx 1 - \left( \frac{32\sigma_0^4 t}{t_0} \right)^{-1/3}, \quad \Gamma_* \approx \left( \frac{4\sigma_0^4 t}{t_0} \right)^{1/6}, \quad (18)$$

which upon integration of  $\beta_*$  yields

$$\xi_* \approx 1 - \frac{2t_0}{t} \left[ 1 + \frac{3}{2^{11/3}} \left( \frac{t}{\sigma_0^2 t_0} \right)^{2/3} \right] \approx 1 - \frac{2t_0}{t}, \quad (19)$$

thus confirming the validity of equation (16) for  $t \ll \sigma_0^2 t_0$ .

Therefore, in this regime, the mean Lorentz factor of the shell follows the law  $\langle \Gamma \rangle \propto t^{1/3}$ . Moreover, for  $t = t_0$ , equation (17) gives  $\Gamma(\xi_*) \sim \sigma_0^{1/3}$  in agreement with the results obtained in Section 2.1. Thus, we may conclude that

$$\langle \Gamma \rangle \approx \left( \frac{\sigma_0 t}{t_0} \right)^{1/3}. \quad (20)$$

This regime continues until the magnetic and kinetic energies become comparable (and  $\Gamma_{\text{ms}} \simeq 1$ ), which implies  $\langle \sigma \rangle \simeq 1$  and  $\langle \Gamma \rangle \simeq \sigma_0$ . This occurs at the time

$$t_c = t_0 \sigma_0^2, \quad (21)$$

after which the shell starts coasting at a constant Lorentz factor  $\langle \Gamma \rangle \simeq \sigma_0$  (as described in Section 3.3).

In Appendix C, we provide an alternative derivation of equation (17), based on the explicit solution of the self-similar rarefaction wave. Furthermore, analytic expressions are derived for the rest mass  $M_*$ , kinetic energy  $E_{\text{kin}}$ , electromagnetic energy  $E_{\text{EM}}$  and total energy (excluding rest energy)  $E_*$  in the region between the head of the secondary rarefaction wave and the vacuum interface:  $\xi_*(t) < \xi < \xi_h = 2[\sigma_0(1 + \sigma_0)]^{1/2}/(1 + 2\sigma_0)$ , as a function of  $\xi_*(t)$ . Together with equation (C8) for  $t(\xi_*)$ , these quantities can be parametrically expressed as a function of the time  $t$  and are presented in Fig. 3 for  $\sigma_0 = 10^2, 10^3$  and  $10^4$  (presumably covering the range of values most relevant for GRBs). Similarly, we also derive the average values (weighted over the energy, according to equation B1) of  $\Gamma$  ( $\langle \Gamma \rangle_*$ ) and  $\sigma$  ( $\langle \sigma \rangle_*$ ) within this region, which are shown in the bottom panel of Fig. 3 for  $\sigma_0 = 10^3$ , along with  $\Gamma(\xi_*)$  and  $\sigma(\xi_*)$ .

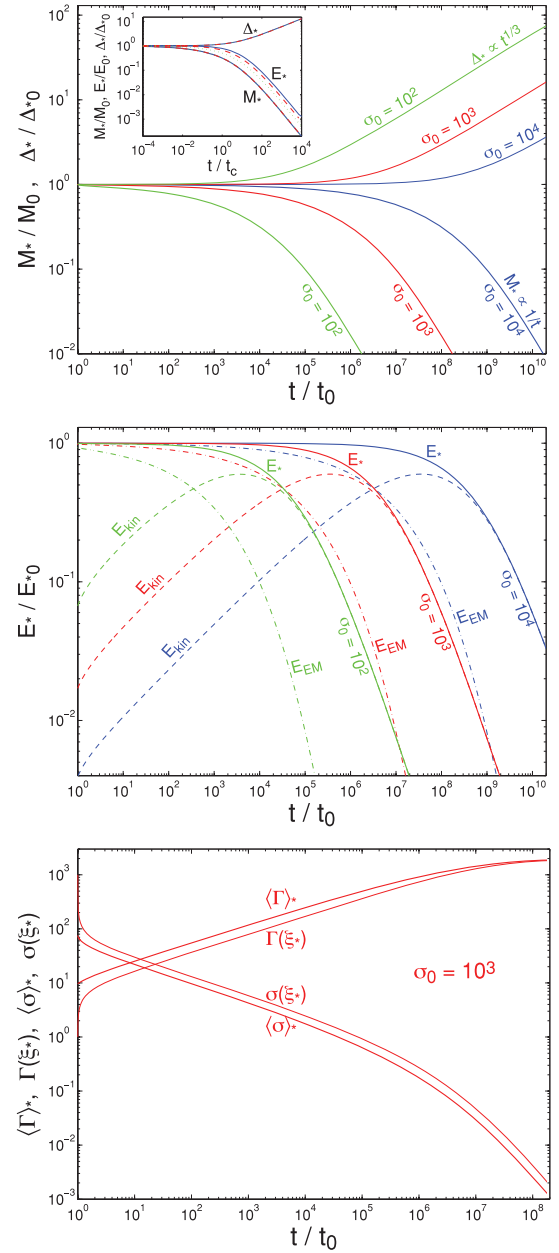
One can see that up to the time  $t \sim t_c = \sigma_0^2 t_0$ , the shell width,  $\Delta_*$ , and total energy,  $E_*$ , remain almost unchanged, with  $\Delta_* \approx 2l_0$  and  $E_*$  being equal to the total (excluding rest energy) energy in the initial solution,  $E_{*0} = E_{\text{EM},0} = (\sigma_0/2)M_0 c^2$ . At the same time, the shell's total mass (and magnetic flux) slowly decreases due to the gradual advance of the secondary rarefaction into the shell. At  $t \ll t_c$ ,  $\langle \Gamma \rangle_*$  is slightly larger than  $\Gamma(\xi_*)$  (with the same scaling  $\propto t^{1/3}$ ), as expected, while  $\langle \sigma \rangle_*$  is slightly lower than  $\sigma(\xi_*)$  even for  $t \gg t_c$ .

The shell's magnetic energy is gradually converted into its kinetic energy:  $E_{\text{kin}} \sim \langle \Gamma \rangle M_0 c^2 \sim E_0(t/t_c)^{1/3}$  at  $t \ll t_c = \sigma_0^2 t_0$ , as  $\langle \Gamma \rangle \approx (\sigma_0 t/t_0)^{1/3}$  in this regime. At  $t \simeq 0.03 t_c$ , these energies become comparable, while  $\sigma(\xi_*)$  and  $\langle \sigma \rangle_*$  drop below unity at  $t/t_c \approx 0.086$  and  $0.037$ , respectively. At  $t > t_c$ , the shell begins to experience significant spreading [ $\Delta_*/\Delta_{*0} \approx 2^{-7/3} 3(t/t_c)^{1/3}$  at  $t \gg t_c$ ]. Its total mass and energy significantly decrease, indicating that the region between vacuum and the secondary rarefaction no longer represents the shell evolution.

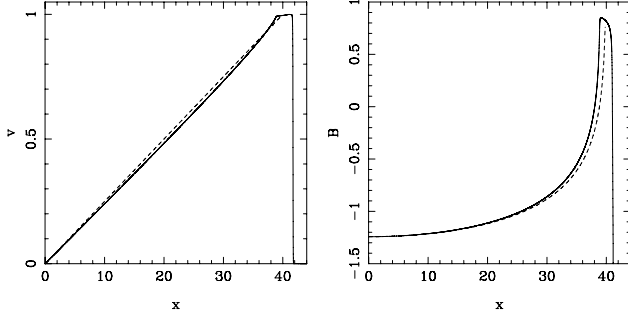
The numerical solution presented in Fig. 2 suggests self-similar evolution with a characteristic linear profile for the flow velocity,  $v \simeq x/t$ , for the region between the wall and the shell (we will refer to this region as the shell's tail). This is expected in the limit where the separation between the shell and the wall becomes much larger compared to  $l_0$ , the only characteristic length-scale of the problem. As shown in Appendix E, such similarity solution does exist,

$$v = \xi, \quad \rho = \frac{1}{t} \frac{C_1}{\sqrt{1 - \xi^2}}, \quad B = \frac{1}{t} \frac{C_2}{1 - \xi^2}, \quad (22)$$

where  $\xi = x/t < 1$  and  $C_i$  are constants. Fig. 4 compares the similarity solution with the numerical solution at  $t = 40$  ( $\sigma_0 = 30$ ). One can see that there is a reasonably good agreement between them. The first equality in equation (22) shows that each fluid element moves with constant speed. This implies that the kinetic energy for any section  $[\xi_1, \xi_2]$  of the solution is conserved. However, the magnetic energy of such a section decreases as  $\propto t^{-1}$ . This indicates that the magnetic energy is transferred along the solution towards



**Figure 3.** Evolution of the shell, corresponding to the region between the front of secondary rarefaction wave ( $\xi_*$ ) and vacuum interface ( $\xi_h$ ), for three different values of the initial magnetization:  $\sigma_0 = 10^2$  (green lines),  $\sigma_0 = 10^3$  (red lines) and  $\sigma_0 = 10^4$  (blue lines). The top panel shows the width of this region,  $\Delta_*$ , and the rest mass,  $M_*$ , within it, both normalized by their initial values at  $t = t_0$  (when the original rarefaction wave is secondary by the wall), as a function of  $t/t_0$ . The magnetic flux,  $\int B dx$ , has exactly the same evolution as the total rest mass. The inset shows these quantities as well as the total energy (kinetic+magnetic)  $E_*$  within this region, normalized by its initial value at  $t = t_0$ ,  $E_{*0} = E_{\text{EM},0} = (\sigma_0/2)M_0 c^2$ , as a function of  $t/t_c$  (where  $t_c = \sigma_0^2 t_0$ );  $\sigma_0 = 10^2, 10^3$  and  $10^4$  are plotted with the dotted, dashed and solid lines, respectively. The curves for  $M_*/M_0$  and  $\Delta_*/\Delta_{*0}$  are practically on top of each other, while those for  $E_*/E_{*0}$  are slightly offset, indicating a slower convergence in the limit  $\sigma_0 \rightarrow \infty$ . The middle panel shows the evolution of  $E_*/E_{*0}$  (thick solid lines), and its decomposition into kinetic (dashed lines) and electromagnetic (dot-dashed lines) energies. The bottom panel shows for  $\sigma_0 = 10^3$  the evolution of the average values (weighted by energy – equation B1) of  $\Gamma$  ( $\langle \Gamma \rangle_*$ ) and  $\sigma$  ( $\langle \sigma \rangle_*$ ) within this region (thick lines), as well as their values at the head of the secondary rarefaction wave ( $\xi_*$ ; thin lines).



**Figure 4.** Numerical and self-similar solutions for shell's 'tail'. The left-hand panel shows the velocity and the right-hand panel shows the magnetic field  $B$ . The numerical solution is represented by the solid lines and the self-similar solution (equation 22) is represented by the dashed lines. The problem parameters and units are the same as in Fig. 1. The time is  $t = 40$  and the numerical solution is shifted along the  $x$ -axis so that the wall is now located at  $x = 0$ .

$\xi = 1$ , where this solution is no longer applicable (as  $\xi = 1$  implies  $\Gamma = \infty$ ). In order to confirm this conclusion, consider a conserved  $Q$  that satisfies equation

$$\frac{\partial Q}{\partial t} + \frac{\partial F}{\partial x} = 0.$$

Next consider a fluid element bounded by  $x_1 = \xi_1 t$  and  $x_2 = \xi_2 t$ . The amount of  $Q$  held by this element,

$$Q(\xi_1, \xi_2, t) = \int_{\xi_1 t}^{\xi_2 t} Q(x, t) dx,$$

satisfies the equation

$$\frac{d}{dt} Q(\xi_1, \xi_2, t) = \bar{F}(\xi_1, t) - \bar{F}(\xi_2, t)$$

where

$$\bar{F} = F - \xi Q$$

is the flux of  $Q$  through the boundary moving with speed  $\xi$ . For the energy,

$$\bar{F}_e = \frac{b^2}{2} v = \frac{(B/\Gamma)^2}{8\pi} v = \frac{C_2^2}{8\pi t^2} \frac{\xi}{1 - \xi^2},$$

which represents the work per unit area and time done by the fluid behind  $\xi$  on the fluid ahead of  $\xi$  [the force per unit area is simply the magnetic pressure,  $f = b^2/2$ , and thus  $dW = f dx = (b^2/2) v dt$ ]. This is a positive and monotonically increasing function of  $\xi$ , which implies transport of energy through the tail towards the shell ( $\xi = 1$ ), in the direction of motion of the flow. Clearly this is due to the work done by the magnetic pressure during the tail's spreading. In the tail's head, this energy is presumably converted into the kinetic energy.

At late times after most of the magnetic energy is transformed into kinetic energy, this solution may still reasonably describe the tail of the flow, corresponding to ballistic motion at  $\Gamma \ll \sigma_0$ . It implies that in the tail, there is approximately equal rest mass per decade in  $\Gamma$ :  $dM/d \ln \Gamma = C_1/\beta$ ,  $dM/d \ln u = C_1/\beta$  and

$$M(< \beta) = \frac{C_1}{2} \ln \left( \frac{1 + \beta}{1 - \beta} \right) = C_1 \ln [\Gamma(1 + \beta)],$$

and equal energy per unit four-velocity,  $dE/du = C_1$  or  $E(< u) = dE/d \ln u = C_1 u \propto u$ , so that most of the energy is carried by the fastest material. In other words, deep in the tail, there is a good part of the total rest mass, but a very small fraction of the total energy.

### 2.3 Numerical simulations

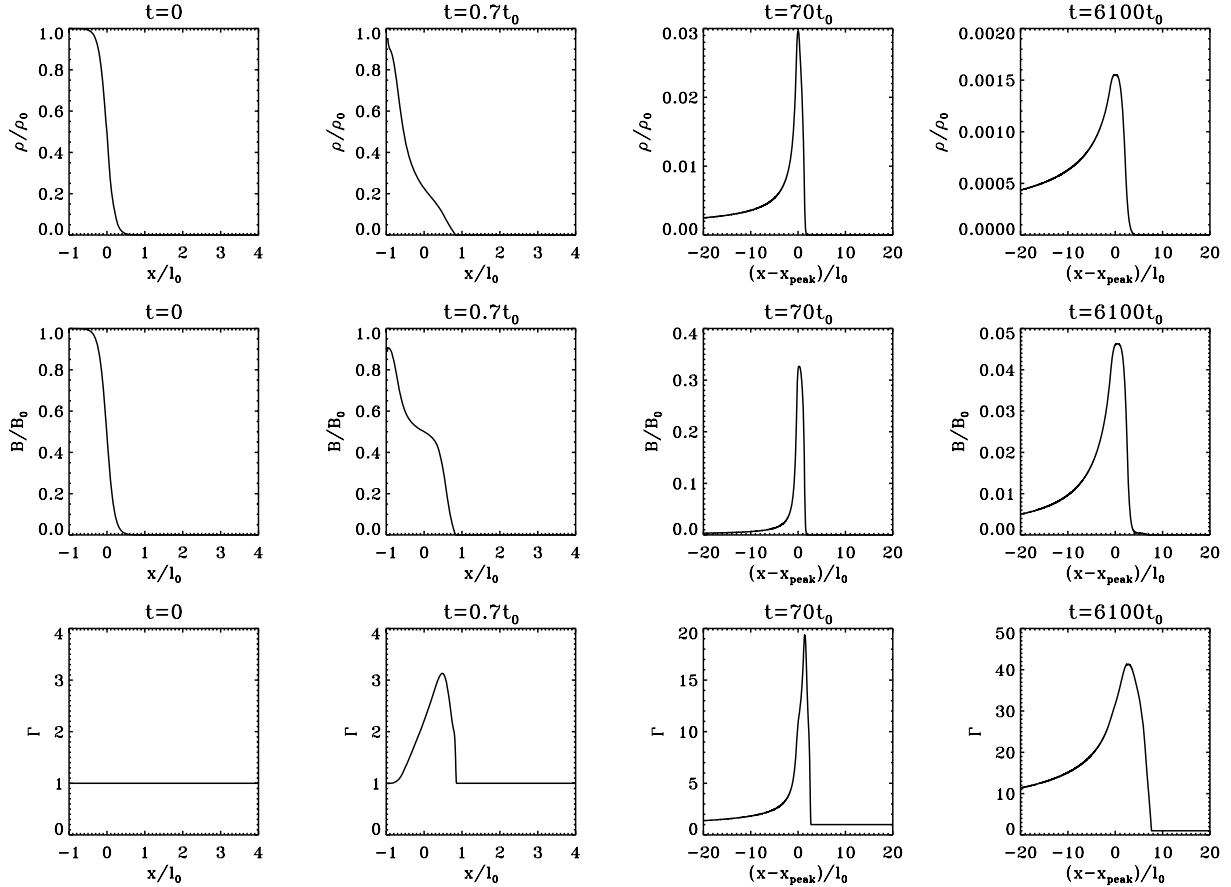
In order to test the validity of our conclusions, we have carried out numerical simulations for the evolution of a cold finite shell, initially highly magnetized and at rest, as it expands into vacuum. We numerically integrate the relativistic magnetohydrodynamic (RMHD) equations (A1) and (A2) in the cold limit, where the gas pressure is set to zero. As shown in Appendix D, the equations in spherical coordinates can be reduced to the planar case, so it suffices to find the solution in the Cartesian one-dimensional geometry.

**Short-term evolution:** first, in order to validate our analytic treatment in Section 2.2, we used exactly the same initial conditions as used in our analytic test case, namely a perfectly uniform, cold and highly magnetized shell at rest. At  $t = 0$  the shell occupies the region  $-l_0 < x < 0$ , where at  $x = -l_0$  it is bounded by a solid wall and in the region  $x > 0$  there is vacuum. The magnetic field is aligned with the  $y$ -direction. We have used the initial magnetization of  $\sigma_0 = 30$ .

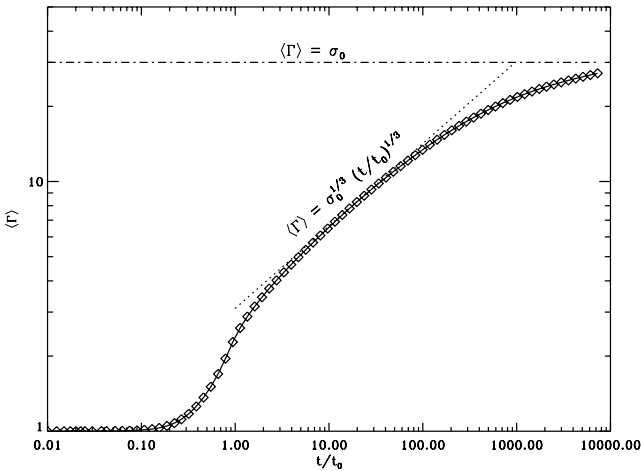
In agreement with our analytic analysis, the shell separates from the wall at dimensionless time  $t \approx t_0$  when its thickness in the laboratory frame is  $\Delta \approx 2l_0$ . After this time, the solution can be described as a shell of constant thickness  $\Delta \approx 2l_0$  followed by a low-energy tail (see Fig. 2, which shows the solution at  $t = 20t_0$ ). In the tail of the flow, the velocity  $v_x$  grows linearly with  $x$  as predicted in the self-similar solution (see Appendix E).

**Long-term evolution:** next we set out to test the long-term evolution. We used slightly modified initial conditions: a shell of width  $l_0$  with roughly constant density and magnetic field, corresponding to a constant magnetization of  $\sigma_0 = 30$ , whose back end touches a reflecting wall on the left-hand side (at  $x = -l_0$ ) and is tapered off to vacuum with a hyperbolic tangent profile on the right-hand side over a thickness  $l_0/10$ , that is, at  $t = 0$  and  $x > -l_0$ , we have  $\rho/\rho_0 = (B/B_0)^2 = [1 - \tanh(10x/l_0)]/2$  and  $\sigma = B^2/4\pi\rho c^2 = B_0^2/4\pi\rho_0 c^2 = \sigma_0$ . We use a simple second-order accurate Harten, Lax and van Leer scheme with Runge–Kutta third-order time-integration for the numerical algorithm. The resolution is 100 cells per  $l_0$  and the Courant number is 0.25. To follow the evolution of the relativistically moving shell for long times without enlarging the grid, we implemented a 'moving window' algorithm, where all quantities are shifted to the left-hand side by  $c\Delta t_{\text{shift}}$  cells every  $\Delta t_{\text{shift}} = 200$  time-steps. Thus, the simulation frame effectively flies to the right-hand side at the speed of light and the left-hand wall becomes causally disconnected from the main domain. The moving window algorithm turns on after the shell moves away from the reflecting wall by about  $70l_0$ . The size of the moving window domain is  $10^4$  cells corresponding to  $100l_0$ .

Fig. 5 shows the profiles of density, magnetic field and Lorentz factor at several times during the simulation, while Fig. 6 shows the evolution of the energy-weighted average Lorentz factor (defined in equation B1),  $\langle \Gamma \rangle$ , with time. We measure time and space in units of the shell crossing time  $t_0 \approx l_0/c$  and initial shell widths  $l_0$ , respectively. As expected, the evolution has several distinct phases. First, the rarefaction wave propagates towards the reflecting wall, as seen in the first two columns of Fig. 5. The right-hand end of the shell accelerates and  $\langle \Gamma \rangle$  reaches  $\sigma_0^{1/3}$  when the rarefaction wave crosses the shell at  $t = t_0$ . At this point, the shell decouples from the wall. As seen in Fig. 6, at  $t = t_0$ , the evolution of  $\langle \Gamma \rangle$  changes to the accelerating stage, which takes it beyond  $\sigma_0^{1/3}$ , increasing as  $t^{1/3}$ . In this regime, the shell remains thin ( $\sim 2l_0$ , third column in Fig. 5), leaving a low-density tail behind. This is the 'impulsive' stage, where the right-hand part of the shell accelerates at the expense



**Figure 5.** Snapshots of physical quantities from the numerical simulation of the evolution of a highly magnetized shell. Top row: proper density; middle row: magnetic field; bottom row: Lorentz factor. Each column corresponds to different times. Density and magnetic field are normalized by  $\rho_0$  and  $B_0$ , such that  $B_0^2/4\pi\rho_0c^2 = \sigma_0$ . In the third and fourth columns, in order to follow the moving shell, the  $x$ -coordinate is centred on the location  $x_{\text{peak}}$  of the peak of the density of the shell.



**Figure 6.** Time-evolution of the energy-weighted average Lorentz factor of the shell, showing the rarefaction wave, magnetic acceleration and saturation stages.

of the magnetic ‘exhaust’ on the left-hand part. The dotted line in Fig. 6 shows the analytical expectation during this stage,  $\langle \Gamma \rangle = \sigma_0^{1/3} (t/t_0)^{1/3}$ , for the parameters of the simulation. The agreement during the accelerating stage is very good.

In the saturation (or coasting) stage, which starts around  $t/t_0 \gtrsim \sigma_0^2$ , the shell starts to spread significantly in the laboratory frame (last column in Fig. 5). The evolution of  $\langle \Gamma \rangle$  deviates from the earlier  $t^{1/3}$  power law and begins to approach the asymptotic value  $\langle \Gamma \rangle = \sigma_0$  (dot-dashed line in Fig. 6), corresponding to the complete conversion of magnetic to kinetic energy in the shell.<sup>7</sup> In the far asymptotic regime, the moving window of the simulation, which flies at the speed of light, begins to outrun the shell, which moves with finite Lorentz factor. Thus, the last points in the evolution in Fig. 6 can be affected by the fact that a significant fraction of the shell material is left outside the moving window. However, the trend for saturation is clear. Overall, our simulations support very well the analytical arguments about the rarefaction wave, impulsive acceleration and the saturation (or coasting) stages of the evolution of an impulsive flow. We have also experimented with larger values of  $\sigma_0 = 100$  and 1000 of the shell. We find that the  $t^{1/3}$  evolution is robust and is seen in both of these cases; however, we did not run the simulations long enough to see the ultimate saturation, as

<sup>7</sup> In this asymptotic limit,  $\langle \Gamma \rangle_M \rightarrow 1 + \sigma_0/2$  for the mass-weighted average defined in equation (B3) and the exact asymptotic value for the energy-weighted average  $\langle \Gamma \rangle_E$  defined in equation (B1) depends on the asymptotic distribution of  $dM/d\Gamma$ , which, in turn, depends on the exact initial conditions. It is none the less always  $\sim \sigma_0$ .



the saturation time is much longer, scaling as  $\sigma_0^2$ . We also checked that the evolution is not sensitive to the exact shape of the initial shell.

### 3 ‘BACK OF THE ENVELOPE’ DERIVATIONS

In this section, we re-derive the key results of previous sections using crude but simple calculations, which help to clarify its physics. They also show that this phenomenon is rather generic and not very sensitive to exact initial configuration.

#### 3.1 Initial acceleration

As the shell expands and the flow develops, the electromagnetic part of the solution closely follows that of vacuum electrodynamics. The shell (electromagnetic pulse) thickness increases by a factor of 2, from  $l_0$  to  $l_1 \approx 2l_0$ , and the magnetic field decreases by a factor of 2, from  $B_0$  to  $B \approx B_0/2$ . At the same time, an electric field  $E \approx B$  is generated. Since the flow is still highly magnetically dominated, the energy conservation implies

$$B_0^2 l_0 \sim (E^2 + B^2) l_1 \sim 2B^2 l_1.$$

On the other hand, the mass conservation reads

$$\rho_0 l_0 \sim \rho \Gamma l_1,$$

where  $\rho$  and  $\Gamma$  are the characteristic (‘mean’) density and Lorentz factor, respectively. From this, we find that

$$\frac{B^2}{4\pi\rho\Gamma} \sim \frac{\sigma_0}{2}.$$

Since the fluid frame magnetic field  $B' = B/\Gamma$ , it gives

$$\Gamma\sigma \sim \frac{\sigma_0}{2}.$$

From the MHD viewpoint, the shell separates from the wall (i.e. loses causal contact with it) when its Lorentz factor just exceeds that of the fast-magnetosonic speed, given by equation (2), which corresponds to a four-velocity  $u_{\text{ms}} = \sigma^{1/2}$ . For  $\sigma \gg 1$ , this reads

$$\Gamma \approx \sigma^{1/2}.$$

Combining the last two equations, we find the anticipated results that at  $t_0$  when the shell separates from the wall,

$$\langle \Gamma \rangle \sim \sigma_0^{1/3} \quad \text{and} \quad \langle \sigma \rangle \sim \sigma_0^{2/3}.$$

It is easy to see that these calculations are not sensitive to geometry and apply equally well to planar, spherical and cylindrical shells with a tangential magnetic field.

#### 3.2 Acceleration after the separation

After the separation from the wall, the total momentum of the shell no longer increases and it is mainly in electromagnetic form. However, the shell plasma (corresponding to the front of the flow) continues to be accelerated by the magnetic pressure gradient that has developed during the first phase. (Although, in the laboratory frame, the magnetic field is almost uniform, the magnetic pressure is given by the strength of magnetic field in the comoving frame  $B' = B/\Gamma$ , which is non-uniform.) Similarly, the plasma at the back of the flow (inside the secondary rarefaction wave that develops and propagates into the back of the shell) is decelerated by the magnetic pressure gradient there.

Magnetic flux conservation implies that  $Bl \approx \text{constant}$ , where  $l$  is the shell width. Therefore, the electromagnetic energy scales as

$$E_{\text{EM}} \propto B^2 l \propto l^{-1},$$

and thus it decreases significantly when  $l$  increases significantly, say, doubles its initial value of  $l(t_0) = l_1 \approx 2l_0$ . Since the part of the shell carrying most of the energy has a spread in the Lorentz factor of the order of  $\Delta\Gamma(t) \sim \Gamma(t)$  around its typical value,  $\Gamma(t)$ , it spreads such that its width grows as

$$l \sim l_1 + \frac{t - t_0}{\Gamma^2(t)} \sim l_1 + \frac{t}{\Gamma^2(t)}, \quad (23)$$

where we use units of  $c = 1$  and the last approximate equality holds for  $t \gg t_0$  (factors of the order of unity are dropped for simplicity). Now,  $l$  increases significantly at time  $t_c$  when the two terms on the right-hand side of the above equation become comparable,

$$\frac{t_c}{\Gamma^2(t_c)} \sim l_1 \sim t_0.$$

Since  $t_c$  is also the time when the electromagnetic energy decreases significantly, we know that at  $t_c$  we must have  $\sigma(t_c) \sim 1$  and  $\Gamma(t_c) \sim \sigma_0$ , regardless of the value of  $t_c$ , which we want to derive here. Thus, we find that

$$t_c \sim t_0 \Gamma^2(t_c) \sim t_0 \sigma_0^2.$$

We have already derived in the previous subsection that  $\Gamma(t_0) \sim \sigma_0^{1/3}$  and therefore if indeed  $\Gamma$  increases as a power law with time  $t$  between  $t_0$  and  $t_c$  (which is the only viable option), then the power-law index must be

$$\frac{d \log \Gamma}{d \log t} = \frac{\log[\Gamma(t_c)/\Gamma(t_0)]}{\log(t_c/t_0)} = \frac{\log(\sigma_0^{2/3})}{\log(\sigma_0^2)} = \frac{1}{3}.$$

Thus, we obtain the anticipated scaling  $\Gamma \propto t^{1/3}$  at  $t_0 < t < t_c$ . Since  $\Gamma(t_0) \sim \sigma_0^{1/3}$ , this implies

$$\Gamma(t_0 < t < t_c) \sim \left( \frac{\sigma_0 t}{t_0} \right)^{1/3}.$$

An alternative derivation is provided in Appendix F. Thus, the scalings obtained for the test case of an initially uniform shell are in fact rather generic.

#### 3.3 Coasting phase and summary of main results

At  $t > t_c$ , the flow essentially becomes unmagnetized (i.e. with a low magnetization,  $\sigma < 1$ ), its internal (magnetic) pressure becomes unimportant dynamically, and each fluid element within the shell coasts at a constant speed (ballistic motion). The shell coasts at a typical Lorentz factor of  $\Gamma \sim \sigma_0$ , where the expansion of the shell during its acceleration stage results in a dispersion  $\Delta\Gamma \sim \Gamma$  in its Lorentz factor (i.e. that of the part of the shell carrying most of the energy) around this value. This causes an increase in the shell width in the laboratory frame, according to equation (23), where at  $t > t_c$ , the second term on the right-hand side becomes dominant, resulting in

$$\frac{l}{l_1} \approx \frac{l}{2l_0} \sim \begin{cases} 1 & \zeta_c < 1, \\ \zeta_c & \zeta_c > 1, \end{cases} \quad (24)$$

where  $\zeta_c = t/t_c \approx R/R_c$ , while  $t_c = t_0 \sigma_0^2$  and  $R_c \approx t_c$  are the coasting time and radius, respectively. Since  $E_{\text{EM}} \propto l^{-1}$  and at  $t > t_c$ ,  $E_{\text{kin}} \approx E = \text{constant}$ ,  $\sigma = E_{\text{EM}}/E_{\text{kin}} \propto l^{-1} \propto t^{-1}$ . One can summarize this

result in terms of the laboratory frame time or the distance  $x \approx ct$  of the shell from the wall (or source), either in terms of  $\zeta_c$ ,

$$\langle \Gamma \rangle \sim \begin{cases} \sigma_0 \zeta_c^{1/3} & \sigma_0^{-2} < \zeta_c < 1, \\ \sigma_0 & \zeta_c > 1, \end{cases} \quad (25)$$

$$\langle \sigma \rangle \sim \begin{cases} \zeta_c^{-1/3} & \sigma_0^{-2} < \zeta_c < 1, \\ \zeta_c^{-1} & \zeta_c > 1, \end{cases} \quad (26)$$

or in terms of  $\zeta_0 = t/t_0 \approx R/R_0$ ,

$$\langle \Gamma \rangle \sim \begin{cases} (\sigma_0 \zeta_0)^{1/3} & 1 < \zeta_0 < \sigma_0^2, \\ \sigma_0 & \zeta_0 > \sigma_0^2, \end{cases} \quad (27)$$

$$\langle \sigma \rangle \sim \begin{cases} \sigma_0^{2/3} \zeta_0^{-1/3} & 1 < \zeta_0 < \sigma_0^2, \\ \sigma_0^2 \zeta_0^{-1} & \zeta_0 > \sigma_0^2. \end{cases} \quad (28)$$

#### 4 SELF-ACCELERATION: A PARADOX?

The apparent self-acceleration of the plasma shell, which was described in Sections 2 and 3, is rather unusual and even somewhat perplexing. This self-acceleration reminds of the outrageous tall tales of Baron Munchausen, particularly the one where he escapes from a swamp by pulling himself up by his own hair (or bootstraps). In this section, we try to resolve this apparent paradox and clarify how the shell keeps significantly accelerating after losing causal contact with the wall.

At the heart of the apparent paradox lies the well-known fact that for a closed system with no external forces, the centre of momentum (CM) velocity,  $\beta_{\text{CM}}$ , remains constant. This is valid not only in the Newtonian regime, but also in special relativity, where  $\beta_{\text{CM}}$  is the velocity of an inertial frame,  $S_{\text{CM}}$ , where the total momentum of the system vanishes,  $P' = 0$ , as measured simultaneously in that frame.<sup>8</sup> If we denote the energy and momentum as measured in  $S_{\text{CM}}$  by  $E'$  and  $P' = 0$ , then in an inertial frame  $S$  in which  $S_{\text{CM}}$  moves at a velocity  $\beta_{\text{CM}} = \beta_{\text{CM}} \hat{x}$ , and the total energy and momentum are  $E$  and  $P$ , respectively, a simple Lorentz transformation implies  $P_z = P'_z = 0$ ,  $P_y = P'_y = 0$ , and

$$P = P_x = \Gamma_{\text{CM}}(P'_x + \beta_{\text{CM}} E') = \Gamma_{\text{CM}} \beta_{\text{CM}} E',$$

$$E = \Gamma_{\text{CM}}(E' + \beta_{\text{CM}} P'_x) = \Gamma_{\text{CM}} E', \quad \implies \quad \beta_{\text{CM}} = \frac{P}{E}. \quad (29)$$

Since in the absence of external forces,  $P$  and  $E$  remain constant, as measured in frame  $S$ , so does  $\beta_{\text{CM}}$ .

Now, for simplicity, let us consider a slight variation in our simple test case from Section 2, where at the moment the original rarefaction wave reaches the wall (i.e. at  $t = t_0$  in the laboratory frame, which is identified with frame  $S$  here): the wall is removed (and replaced by vacuum). This modification should not have any effect on the propagation speed and location of the head of the secondary rarefaction wave,  $\beta_* = dx_*(t)/dt$  and  $\xi_*(t) = x_*(t)/t$ , or on the flow ahead of it, at  $\xi > \xi_*(t)$ . It would affect only the region behind the head of the secondary rarefaction wave. Therefore, it should not affect the local dynamics of the ‘shell’ [where the shell refers to  $\xi_*(t) < \xi < \xi_h = \beta_{\text{max}}$ ]. However, in this case, at  $t > t_0$ , there is immediately no external force exerted on the flow, and therefore its

total momentum and energy are fixed to their values at  $t = t_0$  (for the energy, this was true also before  $t_0$ , since the wall was static in the laboratory frame):

$$P(t \geq t_0) = P(t_0) = \int_0^{t_0} F dt = \frac{B_0^2}{8\pi} t_0 = M_0 \frac{\sqrt{\sigma_0(1+\sigma_0)}}{2},$$

$$E(t \geq 0) = M_0 \frac{2 + \sigma_0}{2}, \quad \implies \quad \beta_{\text{CM}} = \frac{\sqrt{\sigma_0(1+\sigma_0)}}{2 + \sigma_0}. \quad (30)$$

where  $M_0 = \rho_0 l_0$  is the total rest mass (which, like  $P$ ,  $E$  and  $F$ , is measured per unit area, given the one-dimensional planar geometry). In terms of the Lorentz factor,

$$\Gamma_{\text{CM}} \equiv (1 - \beta_{\text{CM}}^2)^{-1/2} = \frac{2 + \sigma_0}{\sqrt{4 + 3\sigma_0}} \approx \frac{\sigma_0^{1/2}}{\sqrt{3}} \ll \sigma_0, \quad (31)$$

(the last two approximations hold for  $\sigma_0 \gg 1$ ). In Appendix G, we derive the same result for  $\beta_{\text{CM}}$  and  $\Gamma_{\text{CM}}$  by calculating the total momentum in a general rest frame (simultaneously in that frame) and then requiring that it vanishes.

In the CM frame,  $S_{\text{CM}}$ , the total energy is

$$E' = \frac{E}{\Gamma_{\text{CM}}} = \frac{\sqrt{4 + 3\sigma_0}}{2} M_0 \approx \frac{\sqrt{3}}{2} \sigma_0^{1/2} M_0, \quad (32)$$

that is, a factor of  $\sim \sigma_0^{1/2} \gg 1$  larger than the rest energy. Therefore, at late times, when all of the magnetic energy is converted into kinetic energy, the typical Lorentz factor of fluid in this frame must be  $\sim \sigma_0^{1/2}$  and in particular

$$\langle \Gamma' \rangle_M = \frac{E'}{M_0} = \frac{\sqrt{4 + 3\sigma_0}}{2} \approx \frac{\sqrt{3}}{2} \sigma_0^{1/2}. \quad (33)$$

However, since  $P' = 0$ , this implies that comparable fractions (of the order of one-half) of the rest mass would be moving at  $u' \sim \sigma_0^{1/2}$  and at  $u' \sim -\sigma_0^{1/2}$ , corresponding to  $\Gamma \sim \sigma_0$  and  $\Gamma \sim 1$ , respectively, in the laboratory frame. This picture is supported by a direct calculation in the CM frame (for details, see Appendix G and in particular the discussion around Fig. G2).

This bares a lot of resemblance to the simple mechanical analogy that is described in Appendix F, of two masses,  $m$ , initially moving together with a Lorentz factor  $\Gamma$  in the laboratory frame, and connected by a compressed ideal massless spring with potential energy  $E'_{\text{pot}}$  in their initial rest frame. The spring is then released and fully converts its potential energy into kinetic energy of the two masses. In our case, we can take  $m = M_0/2$  and  $E'_{\text{pot}} = E' - M_0$ , so that the final Lorentz factor of each mass is  $\Gamma_* = E'/M_0$  in their original rest frame. Their velocities are parallel and anti-parallel to their original direction of motion relative to the laboratory frame, denoted by subscripts ‘+’ and ‘−’, respectively. If we choose  $\Gamma = \Gamma_{\text{CM}}$ , then  $\Gamma_* = \sqrt{4 + 3\sigma_0}/2$  is slightly larger than  $\Gamma_{\text{CM}}$  resulting in  $\Gamma_+ \approx \sigma_0$  and  $\beta_- \approx -5/13$ . Alternatively, we could choose  $\Gamma = \Gamma_* \neq \Gamma_{\text{CM}}$ , so that the mass at the back would be at rest in the laboratory frame:  $\Gamma_- = 1$  and  $\Gamma_+ = \Gamma^2(1 + \beta^2) \approx 2\Gamma_*^2 \approx (3/2)\sigma_0 \sim \sigma_0$  (in this case  $E$  is somewhat larger than in the original case, since we fixed  $E'$  and slightly increased  $\Gamma$ ). In either case, the mass at the front ends up with  $\Gamma_+ \sim \sigma_0$  and carries all (or almost all) of the momentum and kinetic energy in the laboratory frame, while the mass at the back has  $\Gamma_- \sim 1$  and carries a negligible fraction of the total energy and momentum. In the CM frame, however, the two masses have equal energy and momenta of equal magnitude in opposite directions.

Thus, the ‘Baron Munchausen paradox’ described at the beginning of this section is resolved as follows. First, while in the laboratory frame, the typical Lorentz factor at time  $t_0$ , when the original rarefaction wave reaches the wall, is  $\langle \Gamma(t_0) \rangle \sim \sigma_0^{1/3}$ , the CM Lorentz factor is significantly higher,  $\Gamma_{\text{CM}} \sim \sigma_0^{1/2}$ . This difference may be

<sup>8</sup> When viewed from this frame, it is obvious that in the absence of any external force, the total momentum  $P' = 0$  remains unchanged, so this frame remains the CM frame, and its velocity  $\beta_{\text{CM}}$  as measured in any other inertial frame remains constant.

attributed to a simultaneity effect: the Lorentz factor of a rest frame where the total momentum vanishes as measured simultaneously in the laboratory frame at  $t_0$  is indeed  $\sim \sigma_0^{1/3}$ . However, the more physically meaningful definition of the CM frame<sup>9</sup> requires that the momentum be calculated simultaneously in that frame and this accounts for the difference. Secondly, even though  $\Gamma_{\text{CM}}$  remains constant, in accordance with our Newtonian intuition, we argue that the more astrophysically relevant quantity is  $\langle \Gamma \rangle_E$  – the energy-weighted mean value of  $\Gamma$  (in the laboratory frame) – and  $\langle \Gamma \rangle_E$  does increase with time, approaching  $\sim \sigma_0$  at late times ( $t > t_c$ ). This is justified below (and in the discussion around Fig. G2).

It is by now clear that  $\beta_{\text{CM}}$  and  $\Gamma_{\text{CM}}$  remain constant at  $t \geq t_0$ , while  $\langle \Gamma \rangle_E$  grows with time and approaches  $\sim \sigma_0$  at late times. At such late times,  $t \gg t_c = t_0 \sigma_0^2$ , when all of the magnetic energy is converted into kinetic energy,

$$\langle \beta \rangle_E \equiv \frac{\int dE \beta}{\int dE} \longrightarrow \frac{\int dM \Gamma \beta}{\int dM \Gamma} = \frac{P}{E} = \beta_{\text{CM}}. \quad (34)$$

One might therefore ask, why is it more relevant to take the energy-weighted average of  $\Gamma$ ,  $\langle \Gamma \rangle_E$ , rather than that of  $\beta$ ,  $\langle \beta \rangle_E$ , and then derive from it the corresponding value of  $\Gamma$ ,  $(1 - \langle \beta \rangle_E^2)^{-1/2}$ , which approaches  $\Gamma_{\text{CM}}$  at late times. The answer is that  $\langle \Gamma \rangle_E$  is more representative of the Lorentz factor of the material that carries most of the energy in the laboratory frame, which is the frame where all of our observations are made and the external medium is at rest. This can be seen by using the simple mechanical analogy outlined above of two equal masses  $m = M_0/2$  that end up with  $\Gamma_- = 1$  and  $\Gamma_+ \sim \sigma_0$ . In this case  $E_{\pm} = \Gamma_{\pm} m$  and

$$\langle \Gamma \rangle_E = \frac{\Gamma_+^2 + 1}{\Gamma_+ + 1} \approx \Gamma_+ \sim \sigma_0, \quad \langle \beta \rangle_E = \frac{\Gamma_+ \beta_+}{\Gamma_+ + 1}, \quad (35)$$

$$(1 - \langle \beta \rangle_E^2)^{-1/2} = \sqrt{\frac{\Gamma_+ + 1}{2}} = \Gamma_{\text{CM}} \sim \sigma_0^{1/2},$$

so that using  $\langle \beta \rangle_E$  results in  $\Gamma_{\text{CM}} \sim (\Gamma_+ \Gamma_-)^{1/2}$ , which gives too much weight to the mass that ends up at rest ( $\Gamma_- = 1$ ), even though it carries only a very small fraction of the energy in the laboratory frame,  $(\Gamma_+ + 1)^{-1} \sim \sigma_0^{-1} \ll 1$ . On the other hand,  $\langle \Gamma \rangle_E$  is very close to  $\Gamma_+$ , the Lorentz factor of the mass that carries almost all of the energy in the laboratory frame.

The situation where part of a closed system with no external forces is accelerated to large positive velocities at the expense of another part of that system, which attains large negative velocities, is analogous to a rocket. If the rocket + fuel start at rest with no external forces, then the total momentum remains zero all along. The body of the rocket is accelerated to positive velocities, while the burnt fuel is thrown back with large negative velocities. That is why we had originally dubbed the impulsive acceleration of a shell the ‘magnetic rocket’ effect. The analogy is not perfect, however, as rocket acceleration implies a causal connection between the body of the rocket and the exhaust. In the case of the magnetized shell, the decelerated material behind the secondary rarefaction wave is causally disconnected from the forward material. In the self-similar solution, each fluid element is accelerated by the magnetic pressure gradient towards the asymptotic value of  $\Gamma \simeq 2\sigma_0$ . The secondary rarefaction, however, limits the duration of such forward acceleration. As soon as it reaches this fluid element, its forward acceleration

is terminated and replaced by the deceleration forced by the opposite pressure gradient behind this rarefaction. Thus, while the head of the shell continues to accelerate, the CM speed for the whole flow remains unchanged, apart from the slow increase due to the wall effect.

## 5 DISCUSSION

### 5.1 General points

#### 5.1.1 Impulsive versus steady-state acceleration

The main shortcoming of the steady-state magnetic acceleration, which can be successfully overcome in the impulsive regime, is best illustrated in the case of an unconfined spherical outflow. In the steady-state regime, such a flow accelerates effectively only up to the fast-magnetosonic point, where  $\Gamma \sim \sigma_0^{1/3}$  and  $\sigma \sim \sigma_0^{2/3}$ . After this point, the acceleration becomes very slow, with  $\Gamma$  increasing only logarithmically with distance (Tomimatsu 1994; Beskin, Kuznetsova & Rafikov 1998), resulting in Poynting-flux-dominated flows on length-scales of astrophysical interest. In contrast, the impulsive magnetic acceleration allows effective conversion of electromagnetic energy, which leads relatively quickly to a kinetic-energy-dominated flow. During the main phase of acceleration, after the separation from the wall in our test case, the magnetization parameter decreases with distance as  $\sigma \propto R^{-1/3}$  ( $\Gamma \propto R^{1/3}$ ) and then during the coasting phase as  $\sigma \propto R^{-1}$  ( $\Gamma \approx \text{constant}$ ).

The steady-state magnetic acceleration of collimated flows (jets) is generally more effective, leading to higher asymptotic Lorentz factors and lower magnetization compared to the case of an unconfined flow. However, it still leads to asymptotic values of the magnetization parameter of  $\sigma \geq 1$  (Komissarov et al. 2009a; Lyubarsky 2009, 2010). When the pressure distribution of the confining medium is a power law  $p_{\text{ext}} \propto R^{-\alpha}$ , with  $\alpha > 2$ , the external confinement is in fact still rather insufficient. In such conditions, jets quickly develop conical streamlines and do not accelerate efficiently afterwards as the magnetic hoop stress, magnetic pressure and electric force finely balance each other. The asymptotic value of the Lorentz factor is  $\Gamma \approx \min(\sigma_0^{1/3} \theta_j^{-2/3}, \sigma_0/2)$ , where  $\theta_j$  is the asymptotic half-opening angle of the jet, and the corresponding magnetization parameter is  $\sigma \approx \max(\frac{1}{2} \sigma_0^{2/3} \theta_j^{2/3}, 1)$ .

When  $\alpha < 2$ , the shape of a steady-state flow is parabolic,  $r_j \propto R^{\alpha/4}$  (where  $r_j$  is the cylindrical radius), and its Lorentz factor grows as  $\Gamma \propto r_j \propto R^{\alpha/4}$  until reaching  $\Gamma \approx \sigma_0/2$  ( $\sigma \approx 1$ ) after which the acceleration becomes ineffective again (Komissarov et al. 2009a; Lyubarsky 2009, 2010). Additional acceleration mechanisms, such as the impulsive acceleration mechanism discussed in this paper, are needed to produce kinetic-energy-dominated flows. (As we have already mentioned in Section 1,  $\sigma \sim 1$  is still too high for effective shock dissipation.) On the other hand, for  $2 > \alpha > 4/3$ , the steady-state acceleration is faster compared to the impulsive one. However, even if magnetic acceleration initially occurs in a steady-state fashion and then continues in an impulsive fashion, the kinetic-energy-dominated regime would still be reached at the same distance from the source. As we shall see later, such a cooperation of two mechanisms is natural in astrophysical context.

A related issue is the level of variability at which the impulsive mechanism becomes significant. The best-case scenario is when short bursts of activity are separated by rather long quiet periods, so that the length of almost empty space between shells exceeds by an order of magnitude (or more) the shell width. One can then expect that the collisions between shells effectively occur only in the

<sup>9</sup> For example, with the former hybrid definition, the velocity of that frame changes with time and approaches the constant velocity of the proper CM frame only at asymptotically late times.

coasting phase where practically all of the shell energy is in the kinetic form (see Section 3.3). The issue of interaction between multiple shells is best addressed numerically and this is left to a future work. More generally, the maximum fraction of magnetic energy that can eventually be dissipated at standard MHD shocks in a variable flow, generated via the impulsive plasma acceleration mechanism, can be estimated as  $f_B = (\langle B^2 \rangle - \langle |B| \rangle^2) / \langle B^2 \rangle$ . Essentially, this accounts for the decrease in magnetic energy during the transition to uniform magnetic field.<sup>10</sup> This shows that in weakly variable flows, the impulsive mechanism becomes insignificant. However, the observations of AGNs and microquasar jets indicate that violent bursts rather than smooth variability can be more characteristic of their central engines and a similar conclusion can be made regarding the GRB jets from the often-violent variability of their gamma-ray emission. An additional shock dissipation may occur if within a single shell the magnetic field rapidly alternates, like in the striped winds of pulsars. In such a case, the typical gyration radius downstream of the shocks caused by collisions between shells may exceed the stripe separation, leading to fast dissipation of the alternating component of the magnetic field (Lyubarsky 2003b).

Finally, let us address the efficiency of dissipation in the internal shocks. If the source activity duration is  $t_v$  and the duration of the quiet phase between successive shell ejections is  $t_{\text{gap}} \gtrsim t_v$ , then the maximum fraction of the initial magnetic energy that can be converted to other forms (namely kinetic or internal) is  $f_B = (1 + t_v/t_{\text{gap}})^{-1}$ . If we define the mean value of  $\sigma$  as the ratio of the total magnetic to non-magnetic energies, then this implies that  $\langle \sigma \rangle \geq t_v/t_{\text{gap}}$ , when the different subshells collide.<sup>11</sup> However, internal energy is needed in order to power the observed variable emission in GRBs, AGNs or microquasars. The fraction of the kinetic energy that is converted into internal energy at the internal shocks depends on the local value of  $\sigma$  at the shocks (decreasing with increasing  $\sigma$ , especially at low Mach number shocks). Internal shocks between different subshells occur at  $R_{\text{IS}} \sim R_c t_{\text{gap}}/t_v \gtrsim R_c$ , where the mean magnetization of the shell is  $\langle \sigma(R_{\text{IS}}) \rangle \sim t_v/t_{\text{gap}}$ , that is, close to the above lower limit. This suggests that the efficiency of internal energy generation in internal shocks may significantly increase with  $t_{\text{gap}}/t_v$ . However, it could already be quite reasonable even for  $t_{\text{gap}} \sim t_v$  for which  $f_B \sim 0.5$  and even though  $\langle \sigma(R_{\text{IS}}) \rangle \sim 1$ , the magnetization at the head of each subshell is below average (which may improve the efficiency).

### 5.1.2 Effects of geometry

While our test case problem deals with flows with planar symmetry, the effects of geometry are relatively minor. It is easy to verify that the results of the ‘back of the envelope’ calculations of Section 3 remain unchanged for flows with cylindrical and spherical geometry. Appendix D shows the mathematical reason for this – a suitable variable substitution reduces the equations with spherical symmetry to those with the planar symmetry. From the physical point of view, this relative lack of sensitivity to geometry is based on the

fact that the key factor in the impulsive acceleration is the flow expansion in the direction parallel to the direction of motion, whereas the symmetry of the flow mainly regulates the rate of expansion in the transverse direction. Due to the transverse expansion of jets, the transverse magnetic field, which we assume to be dominating, decreases as  $B_\perp \propto r_j^{-1}$ , whereas the specific volume increases as  $V \propto r_j^2$ , where  $r_j$  is the transverse length-scale. The specific electromagnetic energy remains unchanged,  $E_{\text{EM}} \propto B_\perp^2 V \propto r_j^0$ , and hence the transverse expansion does not lead to magnetic acceleration.

### 5.1.3 Test case and astrophysical flows

The initial configuration of our test case problem can be relevant for eruptive astrophysical phenomena involving fast magnetic reconnection and restructuring of magnetic field configurations, like the magnetar bursts (Lyutikov 2003). In many other cases, an astrophysical central engine may operate rather steadily on relatively long time-scales. These scales have to be compared with the time-scale required for the flow, which is powered by the central engine, to reach the fast-magnetosonic point of the steady-state solution. Once the jet propagates beyond this point, its inner part becomes much less affected by the waves, which are generated at the jet head. In particular, if the jet expands into a relatively empty channel, then the rarefaction wave, which propagates in the comoving jet frame only with the fast-magnetosonic speed, will be confined to the jet head and unable to propagate upstream. Therefore, the fraction of the jet affected by this wave will rapidly decrease in time. For such cases, a shell moving with superfast-magnetosonic speed will be a more suitable initial configuration compared to the static shell next to a wall of our test problem.

After the shell of our test problem had separated from the wall, the plasma acceleration was driven by the magnetic pressure gradient that had been developed in the shell prior to its separation. Thus, it is reasonable to investigate whether a similar pressure distribution can develop in the case where there is no wall but the shell is initially moving with a superfast-magnetosonic speed. In this case, two rarefaction waves will be moving into the shell, one from its head and another from its tail. However, due to the properties of relativistic velocity addition, the head rarefaction will be moving across the shell much faster compared to the tail rarefaction, which will almost ‘freeze’ at the shell tail. Indeed, in the laboratory frame, the tail rarefaction propagates with the speed

$$\beta_t = \frac{\beta + \beta_{\text{ms}}}{1 + \beta\beta_{\text{ms}}} \simeq 1 - \frac{1}{8\Gamma^2\Gamma_{\text{ms}}^2}, \quad (36)$$

where the last equality holds for  $\Gamma, \Gamma_{\text{ms}} \gg 1$ . The length of the jet affected by this wave grows at the rate

$$\Delta\beta_t = \beta_t - \beta \simeq \frac{1}{2\Gamma^2}. \quad (37)$$

The head rarefaction propagates with the speed

$$\beta_h = \frac{\beta - \beta_{\text{ms}}}{1 - \beta\beta_{\text{ms}}} \simeq \frac{\Gamma^2 - \Gamma_{\text{ms}}^2}{\Gamma^2 + \Gamma_{\text{ms}}^2} \quad (38)$$

and the length of the jet affected by this wave grows at the rate

$$\Delta\beta_h = \beta - \beta_h \simeq \frac{2\Gamma_{\text{ms}}^2}{\Gamma^2 + \Gamma_{\text{ms}}^2} \gg \Delta\beta_t. \quad (39)$$

Thus, the head rarefaction crosses the shell first and creates the magnetic pressure gradient, which accelerates the shell in the direction of the head, just like in our test case after separation from the wall.

Moreover, in the rest frame of the shell, the head rarefaction starts propagating much earlier than the tail rarefaction (due to

<sup>10</sup> A similar issue arises in the theory of striped pulsar winds, where smooth fast-magnetosonic waves from an oblique rotator eventually steepen into multiple fast shocks and the same estimate can be used to estimate their efficiency (Lyubarsky 2003a).

<sup>11</sup> Before the overall radial extent of the flow increases appreciably, so that the expression  $f_B = (\langle B^2 \rangle - \langle |B| \rangle^2) / \langle B^2 \rangle$ , which is based on a constant total volume, still holds.

simultaneity effects, since they start more or less simultaneously in the laboratory frame), and this is the reason why the tail rarefaction covers only a very small fraction of the shell even though in this frame, the two rarefaction waves propagate at the same speed ( $\beta_{\text{ms}}$ ) in opposite directions. In this frame, at the time the two rarefaction waves meet (very close to the back end of the flow), the configuration is very close to that of our modified test case, where the wall is removed when the head rarefaction wave reaches it. This fact is used later on, in the derivation leading to equations (56) and (57).

Another important issue is whether the space between different ejecta in astrophysical jets can be considered as empty. Indeed, if the jet production is completely interrupted from time to time, then the external gas may rush into the gaps between different ejecta. The speed of such a lateral flow is obviously limited by the speed of light and this sets an upper limit to the distance from the central source above which the gaps can be considered as empty,

$$R_{\text{min}} = ct_v \theta_j^{-1},$$

where  $t_v$  is the variability time-scale of the central engine (assumed to be similar to  $t_{\text{gap}}$ ), and  $\theta_j$  is the jet half-opening angle. (At this distance from the central source, the shell's cylindrical radius is comparable to the length of the gaps between shells.) For GRB jets with  $t_v \gtrsim 4$  ms and  $\theta_j \sim 0.1$ , it gives  $R_{\text{min}} \gtrsim 1.2 \times 10^9$  cm, and for AGN jets with  $t_v \sim 10$  d and  $\theta_j \sim 1^\circ$ , it gives  $R_{\text{min}} \sim 1.5 \times 10^{18}$  cm. The sound speed of the surrounding gas at such distances can be much lower than the speed of light and one may expect the empty gaps to appear at smaller distances than  $R_{\text{min}}$  (Lyutikov & Lister 2010). However, the ejecta will most certainly drive shock waves into the surrounding gas, heating it to higher temperatures near the jet channel. On the other hand, the increased buoyancy of this gas will result in an outflow, which may become a supersonic wind. This will effectively reduce the speed with which this gas expands into the jet openings. In fact, if  $\theta_j > 1/\mathcal{M}_w$ , where  $\mathcal{M}_w$  is the wind Mach number, then the wind gas will be unable to reach the jet axis.

Moreover, the jet may have this kind of protection from the beginning, if the accretion disc produces its own supersonic wind (we assume here that the relativistic jet is driven by a Kerr black hole). Close to the source, where  $\mathcal{M}_w \leq 1$ , the disc wind may still try to fill the polar region, thus creating an obstruction for the re-born jet. However, it could be pushed aside by the jet on the time-scale required for the jet to overtake the wind,  $\sim t_v v_w / (c - v_w)$ , where  $v_w$  is the wind speed. Using the cited variability scales and  $v_w \sim 0.1c$ , we then find that empty gaps may appear already beginning from the distance of  $\sim 10^7$  cm for GRB jets and  $\sim 3 \times 10^{15}$  cm for AGN jets.

An impulsive operation of the central engine may well result in trapping of some amount of weakly magnetized and dense external gas in the gaps of intermittent highly magnetized jets. This gas will then be accelerated by the jet, leading to development of Rayleigh–Taylor instability, turbulence and mixing. Clearly, this important issue requires further investigation.

## 5.2 Application to GRB jets

We start by considering the propagation of a single shell produced during an active phase of central engine of duration  $t_v$ . This time may correspond to the whole duration of gamma-ray burst or to the duration of one of many shells produced during the active phase of its central engine. The exact nature of the jet variability is not known. In the collapsar model for long GRBs and the binary merger models for short GRBs, this may be related to advection of magnetic field with different polarity on to the black hole, similar to what has been

seen in recent numerical simulations (Barkov & Baushev 2011). In any case, the shortest variability time-scale in GRBs is probably given by the ‘viscous’ time of the inner disc. For neutrino cooled discs, this is

$$t_{v,\text{min}} \approx 4 \left( \frac{\alpha}{0.1} \right)^{-6/5} \left( \frac{M}{M_\odot} \right)^{6/5} \text{ ms}, \quad (40)$$

where  $M$  is the black hole mass and  $\alpha$  is the parameter of the  $\alpha$ -disc model (Popham, Woosley & Fryer 1999). In the alternative model of the GRB central engine, which replaces a superaccreting black hole with a millisecond magnetar, the nature of variability has to be different. It could be driven by a violent restructuring of magnetar magnetosphere, for example, rising buoyant magnetic loops and magnetic reconnection. A relatively mild case of such restructuring, with the characteristic time-scale of the order of  $\sim 20$  ms, has been seen in recent numerical simulations of magnetar-driven GRB jets (Komissarov & Barkov 2007). This time-scale gives us one of the characteristic length-scales of this problem, the shell width,

$$l = ct_v = 3 \times 10^8 \left( \frac{t_v}{10 \text{ ms}} \right) \text{ cm}.$$

(We use the name shell rather loosely here to describe the ejecta, which can be rather elongated and better described as a jet close to the central engine.) There are many other important scales in this problem.

As we have already commented on, the initial acceleration of the flow can proceed in a steady-state fashion. This brings into consideration the radius of the light cylinder,  $r_{\text{lc}}$ , the distance to the fast-magnetosonic surface,  $R_{\text{ms}}$ , the distance up to which the steady-state acceleration mechanism remains effective,  $R_s$ , the distance at which the impulsive acceleration mechanism kicks in,  $R_{\text{cr,t}}$ , the coasting distance,  $R_c$ , and finally the distance where the shell begins to decelerate due to the interaction with the interstellar medium or stellar wind gas,  $R_{\text{dec}}$ . There are many unknowns in this problem. In particular, it is difficult to say what is the exact nature of the collimating medium. The jet is unlikely to be in direct contact with the collapsing star. The hot jet cocoon and the wind from an accretion disc are more likely candidates. Let us suppose that the external pressure scales as  $p_{\text{ext}} \propto R^{-2}$ , the most favourable case for the steady-state collimation acceleration mechanism. Then the steady-state jet is parabolic,  $R \propto r^2$  (where  $r$  is the cylindrical and  $R$  is the spherical radius), and beyond the light cylinder,  $r_{\text{lc}} = c/\Omega$ , its Lorentz factor increases as  $\Gamma \sim (r/r_{\text{lc}}) \approx (R/r_{\text{lc}})^{1/2}$  (e.g. Komissarov et al. 2009a). At the fast-magnetosonic surface,  $\Gamma \approx \sigma_0^{1/3}$  and thus this surface is located at

$$R_{\text{ms}} \sim r_{\text{lc}} \sigma_0^{2/3}. \quad (41)$$

If the jet is powered by a rapidly rotating black hole ( $a = 0.9$ ), then  $r_{\text{lc}} \approx 4R_g$ , where  $R_g = GM/c^2$  is the gravitational radius of the black hole. For the typical parameters of GRBs, it gives

$$r_{\text{lc}} = 6 \times 10^5 \left( \frac{M}{M_\odot} \right) \text{ cm} \quad (42)$$

and

$$R_{\text{ms}} = 6 \times 10^7 \left( \frac{\sigma_0}{10^3} \right)^{2/3} \left( \frac{M}{M_\odot} \right) \text{ cm}. \quad (43)$$

Thus, for the time-scale of the central source variability

$$t_v > \frac{R_{\text{ms}}}{c} \approx 2 \left( \frac{\sigma_0}{10^3} \right)^{2/3} \left( \frac{M}{M_\odot} \right) \text{ ms}, \quad (44)$$

the source will be able to produce a steady-state superfast-magnetosonic flow. Since  $\sim 2$  ms is about the shortest time-scale for

the variability of the central engine (see the end of Section 5.1.3), this must always be the case and the effects of steady-state collimation acceleration have to be taken into account.

As the jet propagates into an almost empty channel cleared by the previous ejections, there will be a rarefaction wave in its heads, making its way into the jet. However, it will be occupying only a small fraction of the jet length. Indeed, in the source frame, the speed of this rarefaction is given by equation (38), which for  $\Gamma^2 \gg \Gamma_{\text{ms}}^2$  implies  $\beta_h \simeq 1$ , and thus the jet length grows much faster than the width of the rarefaction wave in its head.

The collimation acceleration becomes ineffective when the jet half-opening angle,  $\theta_j$ , exceeds the Mach angle,  $\theta_M$ , which is given by

$$\sin \theta_M = \frac{1}{\mathcal{M}_{\text{ms}}} = \frac{\Gamma_{\text{ms}} \beta_{\text{ms}}}{\Gamma \beta}, \quad (45)$$

where  $\mathcal{M}_{\text{ms}}$  is the relativistic fast-magnetosonic Mach number. For  $\Gamma \gg \Gamma_{\text{ms}} \gg 1$  and thus  $\theta_M \ll 1$ , this reduces to  $\theta_M \approx \Gamma_{\text{ms}}/\Gamma$  so that the critical half-opening angle is given by

$$\theta_j \sim \theta_M \sim \frac{\Gamma_{\text{ms}}}{\Gamma}, \quad (46)$$

where  $\Gamma_{\text{ms}} \sim \sigma^{1/2} \sim \sigma_0^{1/2} \Gamma^{-1/2}$ . At this point, the Lorentz factor and magnetization parameter of the jet are

$$\Gamma_s \approx \sigma_0^{1/3} \theta_j^{-2/3} \approx 46 \left( \frac{\sigma_0}{10^3} \right)^{1/3} \left( \frac{\theta_j}{0.1} \right)^{-2/3} \quad (47)$$

and

$$\sigma_s \approx (\sigma_0 \theta_j)^{2/3} \approx 22 \left( \frac{\sigma_0}{10^3} \right)^{2/3} \left( \frac{\theta_j}{0.1} \right)^{2/3}, \quad (48)$$

respectively. [The analysis of flows collimated by an external medium with a power-law pressure distribution by Lyubarsky (2009) leads to a result that differs from this one only by a factor of the order of unity.] In principle, both  $\sigma_0$  and  $\theta_j$  can be estimated from observations of GRBs and their afterglows. In particular,  $\sigma_0$  can be determined using the measurements of Lorentz factor via  $\Gamma \leq \sigma_0$ , where the equality corresponds to full conversion of the electromagnetic energy into the bulk motion kinetic energy. The actual location of the point where the jet Mach angle reaches its critical value and the jet enters the freely expanding regime is less certain as it depends on the exact pressure distribution of the confining medium. For  $p_{\text{ext}} \propto R^{-2}$  we have

$$R_s \sim r_{\text{lc}} \Gamma_s^2 \sim r_{\text{lc}} \sigma_0^{2/3} \theta_j^{-4/3} \sim R_{\text{ms}} \theta_j^{-4/3}. \quad (49)$$

For the parameters typical for GRBs, it gives

$$R_s \approx 1.3 \times 10^9 \left( \frac{M}{M_\odot} \right) \left( \frac{\sigma_0}{10^3} \right)^{2/3} \left( \frac{\theta_j}{0.1} \right)^{-4/3} \text{ cm}. \quad (50)$$

This is significantly lower compared to the radius of long GRB progenitors, which is believed to be of the order on the solar radius,  $R_\odot \approx 7 \times 10^{10}$  cm. Beyond  $R_s$  the collimation acceleration is no longer effective.

In order to find the scale at which the impulsive acceleration comes into play, we first need to estimate how long it takes for the head rarefaction to cross the shell. The length of the section of the shell, which is affected by the rarefaction, grows with time at the rate  $\Delta \beta_h$  given by equation (39), corresponding to a crossing time

$$t_{\text{cr,h}} \approx \frac{t_v}{\Delta \beta_h} \approx \frac{t_v}{2} \left[ \left( \frac{\Gamma}{\Gamma_{\text{ms}}} \right)^2 + 1 \right] \approx \frac{t_v}{2} \left( \frac{\Gamma}{\Gamma_{\text{ms}}} \right)^2, \quad (51)$$

where the last equality assumes a super-fast-magnetosonic regime. By this time the shell will propagate the distance

$$R_{\text{cr,h}} \sim ct_{\text{cr,h}} \sim \frac{ct_v}{2} \left( \frac{\Gamma_s}{\Gamma_{\text{ms}}} \right)^2 \sim ct_v \frac{\Gamma_s^2}{\sigma_s} \sim ct_v \theta_j^{-2}. \quad (52)$$

For the typical GRB parameters, it gives

$$R_{\text{cr,h}} \sim 3 \times 10^{10} \left( \frac{t_v}{10 \text{ ms}} \right) \left( \frac{\theta_j}{0.1} \right)^{-2} \text{ cm}. \quad (53)$$

In the frame moving at a Lorentz factor  $\Gamma_s$ , at the time the two rarefaction waves meet (very close to the back end of the shell), the configuration is very close to that of our modified test case at the time when the head rarefaction wave reaches the wall and the wall is removed. The main difference is that the initial magnetization parameter is  $\sigma_s$  and the initial shell width is  $\Gamma_s ct_v$ . Thus, after the passage of the head rarefaction wave, the typical shell Lorentz factor in this frame is

$$\Gamma_* \sim \sigma_s^{1/3} = (\sigma_0 \theta_j)^{2/9}, \quad (54)$$

and the typical value of the magnetization parameter is  $\sigma_{\text{cr,h}} \sim \sigma_s^{2/3} \sim (\sigma_0 \theta_j)^{4/9}$ . Therefore, the shell Lorentz factor in the laboratory frame is

$$\Gamma_{\text{cr,h}} \sim \Gamma_* \Gamma_s \sim \sigma_0^{5/9} \theta_j^{-4/9} \approx 130 \left( \frac{\sigma_0}{10^3} \right)^{5/9} \left( \frac{\theta_j}{0.1} \right)^{-4/9}. \quad (55)$$

This Lorentz factor is only one order of magnitude below the maximum value given by  $\sigma_0$ . In fact, this may still be only a conservative estimate as we have not taken into account the acceleration related to the transverse expansion of the jet when it crosses the stellar surface (Komissarov et al. 2009a; Tchekhovskoy et al. 2009). This additional acceleration may well increase the mean Lorentz factor by a factor of few (in what follows we denote this factor by  $\kappa$ ). This brings the Lorentz factor up to  $\Gamma_{\text{cr,t}} = \kappa \Gamma_{\text{cr,h}}$  and the magnetization parameter down to  $\sigma_{\text{cr,t}} = \sigma_{\text{cr,h}}/\kappa$ . However, even after this, the jet magnetization is still too high for effective shock dissipation.

For simplicity, we assume that the stellar radius  $R_*$ , where  $\Gamma$  increases by a factor of  $\kappa$ , is  $R_* \leq R_{\text{cr,h}} \ll R_{\text{cr,t}}$ , where  $R_{\text{cr,t}}$  is the radius where the tail rarefaction crosses half of the original shell. We now use the similarity between our modified test case at  $t_0$  and the shell in its rest frame prior to the crossing of the head rarefaction (referred to as the shell's 'initial' rest frame) at the time when the head and tail rarefaction waves meet, as discussed below equation (39). Here the shell's 'initial' rest frame would be moving with a Lorentz factor  $\Gamma_f \sim \kappa^{3/2} \Gamma_s$  relative to the laboratory frame, rather than  $\Gamma_s$ . This can be understood from the fact that we require that after the passage of the head rarefaction  $\sigma \sim \sigma_f^{2/3} \sim \kappa^{-1} \sigma_{\text{cr,h}} \sim \kappa^{-1} \sigma_s^{2/3}$ , so that  $\sigma_f \sim \kappa^{-3/2} \sigma_s$  and  $\Gamma_f \sim \sigma_0/\sigma_f \sim \kappa^{3/2} (\sigma_0/\sigma_s) \sim \kappa^{3/2} \Gamma_s$ .

Now, recall that in our test case, significant additional acceleration after the shell separates from the wall (i.e. at  $t > t_0$ ) starts only when the head of the secondary rarefaction wave – identified here with the tail rarefaction wave after it meets the head rarefaction – reaches fluid with  $\Gamma \sim \sigma_0^{1/3}$ , that is,  $\Gamma(\xi_*) \sim \sigma_0^{1/3}$ . This corresponds to  $\xi_* \sim 0$ , that is,  $\xi'_* \sim 0$  in the frame moving at Lorentz factor  $\Gamma_f$  (referred to as the comoving frame), corresponding to the middle of the shell after the passage of the head rarefaction wave. In our original test case, this corresponded to a single dynamical time ( $\approx t_0$  i.e. between  $t = t_0$  and  $t \approx 2t_0$ ), so we did not pay attention to this. The comoving shell width at the time when the two rarefaction waves meet is  $2\Gamma_f ct_v$  and therefore in our present case, it takes the tail rarefaction wave a time  $t'_{\text{cr,t}} \sim \Gamma_f t_v$  to reach  $\xi'_* \sim 0$  in the comoving frame, which corresponds to a time  $t_{\text{cr,t}} \sim \Gamma_f^2 t_v$  in the laboratory frame. This result can also be obtained using equation (37) with

$\Gamma = \Gamma_f, t_{\text{cr},t} \approx t_v/\Delta\beta_t \sim \Gamma^2 t_v \rightarrow \Gamma_f^2 t_v$ . This corresponds to a radius  $R_{\text{cr},t} \sim \Gamma_f^2 c t_v \sim \kappa^3 \sigma_0^{2/3} \theta_j^{-4/3} c t_v$

$$\approx 6.5 \times 10^{11} \kappa^3 \left(\frac{\sigma_0}{10^3}\right)^{2/3} \left(\frac{\theta_j}{0.1}\right)^{-4/3} \left(\frac{t_v}{10 \text{ ms}}\right) \text{ cm}, \quad (56)$$

where the impulsive acceleration with  $\Gamma \propto R^{1/3}$  begins,

$$\Gamma \sim \frac{\sigma_0}{\sigma} \sim \sigma_0 \left(\frac{R}{R_c}\right)^{1/3} \sim \Gamma_{\text{cr},t} \left(\frac{R}{R_{\text{cr},t}}\right)^{1/3}, \quad (57)$$

for  $R_{\text{cr},t} < R < R_c$ . As a consistency check, we verify that it gives  $R_c \sim R_{\text{cr},t}(\sigma_0/\Gamma_{\text{cr},t})^3 \sim R_{\text{cr},t}\sigma_{\text{cr},t}^3 \sim \sigma_0^2 c t_v$ , as it should from the general considerations outlined in Section 3.2.

We find that  $R_{\text{cr},t} \gg R_s$ , which suggests that the steady-state collimation acceleration and the impulsive acceleration are scale-separated. At  $R = R_{\text{cr},t}$ , the ratio of the shell's cylindrical radius,  $r_j = \theta_j R$ , to its width,  $l_j = c t_v$ , is

$$\frac{r_j}{l_j} \approx \kappa^3 \sigma_0^{2/3} \theta_j^{-1/3} = 215 \kappa^3 \left(\frac{\sigma_0}{10^3}\right)^{2/3} \left(\frac{\theta_j}{0.1}\right)^{-1/3}. \quad (58)$$

Thus, ‘shell’ is indeed a suitable name for the flow at the stage of impulsive acceleration. For the typical parameters of GRBs, the coasting radius is given by

$$R_c \sim \sigma_0^2 c t_v \approx 3 \times 10^{14} \left(\frac{\sigma_0}{10^3}\right)^2 \left(\frac{t_v}{10 \text{ ms}}\right) \text{ cm}, \quad (59)$$

and at  $R > R_c$  the shell coasts at  $\Gamma \sim \sigma_0$ , while its magnetization rapidly decreases as  $\sigma \sim R_c/R$ .

Within this model, prompt gamma-ray emission due to dissipation in internal shocks between different shells within the highly variable outflow naturally occurs in the region  $R \sim (1-10)R_c$ . On one hand, the mean plasma magnetization is  $\sigma \sim 1$  at  $R = R_c$  and then it decreases linearly with the distance. Thus, one of the conditions for effective shock dissipation,  $\sigma \ll 1$ , is satisfied in this region. On the other hand, the width of individual shells begins to grow linearly with the distance, allowing their collisions. (For  $R < R_c$ , the shells keep an almost constant width.) Moreover, the variation in the flow Lorentz factor in the coasting regime is rather large,  $\Delta\Gamma \sim \Gamma$ , which may potentially help increase the efficiency of shock dissipation up to  $\sim 10$  per cent (Beloborodov 2000) or even higher (Kobayashi & Sari 2001).

In order to test the viability of our impulsive magnetic acceleration mechanism, the coasting radius,  $R_c$ , has to be compared with the deceleration radius,  $R_{\text{dec}}$ , at which most of the energy is transferred to the swept-up shocked external medium. In the ‘thin’ shell regime (see below), where  $R_c < R_{\text{dec}}$  and  $\Gamma(R_{\text{dec}}) \sim \sigma_0$ ,  $R_{\text{dec}}$  is given by (e.g. Granot 2005):

$$R_{\text{dec}} = \left[ \frac{(3-k)E_{\text{iso}}}{4\pi A c^2 \sigma_0^2} \right]^{1/(3-k)} \\ = \begin{cases} 2.5 \times 10^{16} n_0^{-1/3} E_{\text{iso},53}^{1/3} \sigma_{0,3}^{-2/3} \text{ cm} & k=0, \\ 1.8 \times 10^{13} A_*^{-1} E_{\text{iso},53} \sigma_{0,3}^{-2} \text{ cm} & k=2, \end{cases} \quad (60)$$

for a spherical external rest-mass density profile  $\rho_{\text{ext}} = AR^{-k}$ , where  $\sigma_{0,3} = \sigma_0/10^3$ ,  $E_{\text{iso}} = 10^{53} E_{\text{iso},53}$  is the isotropic equivalent energy in the flow,  $n = n_0 \text{ cm}^{-3}$  is the external number density for a uniform external medium ( $k=0$ ) and  $A = 5 \times 10^{11} A_* \text{ g cm}^{-1}$  for a stellar wind environment ( $k=2$ ). In some GRBs, the afterglow onset time is observed, which is identified with the observed deceleration time,  $t_{\text{dec}} \sim R_{\text{dec}}/2c\Gamma^2(R_{\text{dec}})$ , and may be used to infer the values of  $\Gamma(R_{\text{dec}})$  and  $R_{\text{dec}}$ , typically giving values of  $\Gamma(R_{\text{dec}})$  of a few hundred

and  $R_{\text{dec}} \sim 10^{17} \text{ cm}$  (Sari & Piran 1999; Liang et al. 2010):

$$R_{\text{dec}} = \left[ \frac{(3-k)E_{\text{iso}} t_{\text{dec}}}{2\pi A c (1+z)} \right]^{1/(4-k)} \\ = \begin{cases} 1.0 \times 10^{17} n_0^{-1/4} E_{\text{iso},53}^{1/4} t_{\text{dec},2}^{1/4} \text{ cm} & k=0, \\ 1.8 \times 10^{16} A_*^{-1/2} E_{\text{iso},53}^{1/2} t_{\text{dec},2}^{1/2} \text{ cm} & k=2, \end{cases} \quad (61)$$

where  $t_{\text{dec}}/(1+z) = 100 t_{\text{dec},2} \text{ s}$ . Note, however, that this method has an observational bias towards low values of  $\Gamma(R_{\text{dec}})$  and large values of  $R_{\text{dec}}$  that correspond to large  $t_{\text{dec}}$  values, since small  $t_{\text{dec}}$  values are hard to measure as optical or X-ray follow-up observations usually start at least tens of seconds after the start of the prompt gamma-ray emission. Nevertheless, even though  $\Gamma(R_{\text{dec}})$  is the Lorentz factor of the shocked external medium and it is close to that of the original ejecta only for a Newtonian or mildly relativistic reverse shock (the ‘think shell’ case, where  $t_{\text{dec}} > T_{\text{GRB}}$ ,  $T_{\text{GRB}}$  being the observed duration of the gamma-ray emission from the GRB), even for the ‘thick-shell’ case (where  $t_{\text{dec}} \sim T_{\text{GRB}}$ ), this method gives  $\Gamma(R_{\text{dec}}) \sim \Gamma_{\text{cr}}$  and  $R_{\text{dec}} \sim R_{\text{cr}}$ , which is the correct deceleration radius in this regime (the critical values of the Lorentz factor,  $\Gamma_{\text{cr}}$ , and radius,  $R_{\text{cr}}$ , are provided below). In both regimes,  $t_{\text{dec}} \gtrsim T_{\text{GRB}}$ , so using  $T_{\text{GRB}}$  instead of  $t_{\text{dec}}$  in equation (61) gives  $R_{\text{cr}}$ , which is a lower limit on the value of  $R_{\text{dec}}$ .

Only when  $R_c \lesssim 0.1 R_{\text{dec}}$ , the internal shock mechanism can be sufficiently effective to explain the prompt gamma-ray emission. Equations (40), (59) and (61) show that this is satisfied only when the characteristic variability time-scale of the central engine is not much longer than the viscous time-scale of the inner disc ( $t_v \sim 10^{-2} \text{ s}$ ), even though for  $R_{\text{dec}} \sim 10^{17} \text{ cm}$ ,  $R_c \lesssim 10^{16} \text{ cm}$  requires  $t_v \lesssim 0.3 \text{ s}$  or an observed variability time  $\lesssim 1 \text{ s}$  for a typical redshift of  $z \sim 2$ . For long GRBs, with the mean duration in the source frame of about  $\sim 10 \text{ s}$ , this implies between a few tens to about 1000 of individual shells. For short GRBs, with the mean duration in the source frame of about  $\sim 0.3 \text{ s}$ , this number can be reduced down to between about a few to a few tens. Moreover, it is generally easier to obtain  $R_c < R_{\text{dec}}$  for a uniform external medium than for a stellar wind environment, since  $R_{\text{dec}}$  is typically much smaller for a stellar wind.

Now we briefly discuss the interaction with the external medium and under which conditions it strongly affects the flow (a more detailed analysis will be presented in a separate work). For simplicity, we shall consider a single shell and discard factors of the order of unity. Let us consider a spherical outflow of duration  $t_0$ , radial width  $R_0 \approx c t_0$ , energy  $E$  and luminosity  $L \approx E/t_0$  propagating into a spherical external rest-mass density profile  $\rho_{\text{ext}} = AR^{-k}$  (with  $k < 10/3$ ). The regime where  $R_c < R_{\text{cr}} < R_{\text{dec}}$  (i.e. where at  $R_c$  only a small fraction of the total energy is transferred to the shocked swept-up external medium) corresponds to the well-known ‘thin-shell’ (or initially Newtonian reverse shock) case for the deceleration of a coasting unmagnetized ( $\sigma < 1$ ) shell (Sari & Piran 1995; Sari 1997), which has been investigated in the context of GRBs. Due to the spreading of the shell at  $R > R_c$  (because of a spread  $\Delta\Gamma \sim \Gamma$  in its Lorentz factor), the reverse shock gradually strengthens and becomes mildly relativistic at  $R_{\text{dec}}$  (which in this regime is given by equation 60), where it finishes crossing the shell, and may produce a bright emission that peaks at an observed time  $t_{\text{dec}} \sim (1+z)R_{\text{dec}}/c\sigma_0^2 \sim (R_{\text{dec}}/R_c)T_{\text{GRB}} > T_{\text{GRB}}$  (i.e. after the end of the prompt GRB emission).

For the other ordering of the critical radii,  $R_{\text{dec}} = R_{\text{cr}} < R_c$  (which may occur for large values of  $t_0$  or a stellar wind external medium), the outflow generally never reaches a coasting phase (so  $R_c$  loses its physical meaning as a coasting radius), since the magnetized shell

starts being significantly affected by the swept-up shocked external medium when the latter still has only a small fraction of the total energy. The impulsive acceleration,  $\Gamma \sim (\sigma_0 R/R_0)^{1/3}$ , proceeds from  $R_0$  up to a radius  $R_u \sim R_{cr}(\sigma_0/\Gamma_{cr})^{-4/(10-3k)}$ , where  $\Gamma_{cr} \sim (ER_0/AC^2)^{1/2(4-k)}$  and  $R_{cr} \sim R_0\Gamma_{cr}^2 \sim (ER_0/AC^2)^{1/(4-k)}$ . Then, at  $R_u < R < R_{cr}$ , the typical Lorentz factor of the magnetized shell becomes similar to that of the swept-up external medium,  $\Gamma \sim (L/AC^3)^{1/4}R^{(k-2)/4}$ , and is determined by the pressure balance at the contact discontinuity that separates these two regions. This is a phase of either a modest deceleration (for  $k < 2$ ) or a reduced acceleration (for  $2 < k < 10/3$ ) that occurs while the outflow is still highly magnetized ( $\sigma \gg 1$  for  $R_{dec} \ll R_c$ ). Therefore, there might not be a reverse shock going into the original magnetized outflow, and even if such a shock develops, then it would be very weak and could dissipate only a very small fraction of the total energy. Finally, at  $R_{cr}$  where  $\Gamma \sim \Gamma_{cr}$ , most of the energy is transferred to the shocked external medium (so that in this regime  $R_{dec} = R_{cr}$ ). Therefore, at  $R > R_{cr}$ , the flow approaches the Blandford & McKee (1976) self-similar solution for a spherical constant energy relativistic blast wave going into an unmagnetized external medium.<sup>12</sup> At  $R_{cr}$  the magnetization is still high,  $\sigma(R_{cr}) \sim \sigma_0/\Gamma_{cr}$ , where this generalized ‘thick-shell’ regime ( $R_{dec} = R_{cr} < R_c$ ) corresponds to  $\sigma_0 > \Gamma_{cr}$ , while the ‘thick-shell’ regime ( $R_c < R_{cr} < R_{dec}$ ) corresponds to  $\sigma_0 < \Gamma_{cr}$ .

Altogether, the acceleration of an initially highly magnetized ( $\sigma_0 \gg 1$ ) impulsive outflow via the impulsive effect and its deceleration due to the interaction with the external medium are tightly coupled and cannot be fully treated in isolation. In other words, the magnetic acceleration naturally sets the initial conditions for the interaction with the external medium, and realistically one cannot simply assume any arbitrary initial configuration of the magnetized outflow near the deceleration radius. Moreover, in the highly magnetized ‘thick-shell’ regime, there is an intermediate phase ( $R_u < R < R_{cr} = R_{dec}$ ), where the magnetic acceleration and the deceleration because of the external medium balance each other, resulting either in a reduced acceleration or in a relatively modest deceleration (as outlined above). If the outflow starts highly magnetized, then it can decelerate either in the unmagnetized ‘thin-shell’ regime [with  $\sigma(R_{dec}) \sim R_c/R_{dec} < 1$  for  $\sigma_0 < \Gamma_{cr}$ ] or in the highly magnetized analogue of the ‘thick-shell’ regime [with  $\sigma(R_{dec}) \sim \sigma_0/\Gamma_{cr} > 1$  for  $\sigma_0 > \Gamma_{cr}$ ]. There is no high-magnetization ‘thin-shell’ regime, and in order to be in the low-magnetization ‘thick-shell’ regime, a single-shell flow cannot start highly magnetized ( $\sigma_0 \gg 1$ ).<sup>13</sup>

### 5.3 Application to AGN jets

We can apply the results obtained in the previous section to AGN jets simply via appropriate rescaling. First, the characteristic masses of black holes are higher,  $\sim 10^7$ – $10^9 M_\odot$ . They are radiation cooled

and the corresponding shortest variability time-scale is

$$t_{v,min} \approx 10 \left( \frac{\alpha \delta^2}{10^{-3}} \right)^{-1} \left( \frac{M}{10^8 M_\odot} \right) d, \quad (62)$$

where  $\delta = H_d/R_d$  is the ratio of the disc height to its radius (Shakura & Sunyaev 1973).

Secondly, the Lorentz factors of AGN jets can be measured directly via observation of proper motion of their knots. Such observations (mainly VLBI radio observations) indicate relatively low Lorentz factors, of the order of a few for weak radio sources (Fanaroff–Riley type I) and  $\langle \Gamma \rangle \sim 10$  with a tail extending up to  $\Gamma \sim 50$  for blazars (Lister et al. 2009). The rapid variability of gamma-ray emission from some AGNs suggests the possibility of even higher Lorentz factors ( $\Gamma > 50$ , Aharonian et al. 2007). Assuming that the magnetic acceleration is efficient in these sources and hence the observed  $\Gamma$  is close to  $\sigma_0$ , we obtain a characteristic value of  $\sigma_0 \sim 10$ , which is much lower compared to GRBs. In principle, the value of  $\sigma_0$  can be higher near the black hole and then decrease downstream, for example, as a result of some mass-loading processes. However, at present, we have no concrete evidence for this. Finally, the observed half-opening angles of blazar jets are smaller,  $\sim 1^\circ$ – $3^\circ$  (Pushkarev et al. 2009).

The corresponding rescaling of the results for GRB jets yields the light cylinder radius

$$r_{lc} = 6 \times 10^{13} \left( \frac{M}{10^8 M_\odot} \right) \text{ cm}, \quad (63)$$

the distance to the fast-magnetosonic surface

$$R_{ms} = 2.7 \times 10^{14} \left( \frac{\sigma_0}{10} \right)^{2/3} \left( \frac{M}{10^8 M_\odot} \right) \text{ cm}, \quad (64)$$

and the shortest variability time-scale required for establishing a steady-state superfast-magnetosonic flow

$$t_v > 2.5 \left( \frac{\sigma_0}{10} \right)^{2/3} \left( \frac{M}{10^8 M_\odot} \right) \text{ h}. \quad (65)$$

Since the time-scale of strong central engine variability is unlikely to be shorter than the viscous time-scale of the inner accretion disc,

$$t_{vis} \sim 100 R_g/c \sim 1.0 \left( \frac{M}{10^8 M_\odot} \right) d,$$

we conclude that, just like in the case of GRBs, the initial acceleration of AGN jets up to superfast-magnetosonic speeds is provided in a steady-state fashion. Moreover, the recent observations of AGN jets (Pushkarev et al. 2009) clearly indicate that they satisfy the  $\Gamma\theta_j < 1$  condition of effective steady-state collimation acceleration (Komissarov et al. 2009a). The observed decrease in the half-opening angle with distance in the M87 jet also supports the theory of collimation acceleration (Biretta, Junor & Livio 2002; Gracia, Tsinganos & Bogovalov 2005).

The distance at which one-half of the electromagnetic energy is converted into the energy of bulk motion is now

$$R_s \approx 0.02 \left( \frac{M}{10^8 M_\odot} \right) \left( \frac{\sigma_0}{10} \right)^{2/3} \left( \frac{\theta_j}{1^\circ} \right)^{-4/3} \text{ pc} \quad (66)$$

(see also Komissarov et al. 2007). This scale is unresolved with modern VLBI systems. The recent numerical simulations show that the collimation acceleration may continue a bit beyond this point, reducing the magnetization down to  $\sigma \sim 0.4$  within another decade of distance from the source (Komissarov et al. 2007). This is still a relatively high magnetization leading to relatively low efficiency of MHD shock dissipation. Additional impulsive acceleration can

<sup>12</sup> The previous regime,  $R_u < R < R_{cr}$  corresponds to another variant of that solution, with energy injection into the shocked external medium by a relativistic wind from the central source.

<sup>13</sup> This might still be possible, under favourable conditions, for a highly variable flow with a large number of high-contrast subshells that accelerate independently, and then quickly collide and merge into a wider shell via internal shocks, soon after reaching their coasting radius and  $\sigma < 1$ . This would amount to quasi-continuous energy injection by subsequent subshells just after the deceleration radius of the first subshell, thus increasing the deceleration radius of the whole flow.



improve this. This time, however, when the impulsive mechanism switches on, this is already the coasting regime. Indeed, the fast-magnetosonic speed corresponding to  $\sigma = 0.4$  is  $\beta_{\text{ms}} \sim 0.5$ . Instead of equation (38) the speed of the head rarefaction is then given by

$$\beta_h \sim \frac{2\Gamma^2 - 2}{2\Gamma^2 + 1} \quad (67)$$

and the length of the section of the shell affected by the rarefaction grows with time at the rate

$$\begin{aligned} \Delta\beta_h &= \beta - \beta_h = \beta_{\text{ms}}/[\Gamma^2(1 - \beta\beta_{\text{ms}})] \\ &\approx \Gamma^{-2}\beta_{\text{ms}}/(1 - \beta_{\text{ms}}) \sim \Gamma^{-2}, \end{aligned} \quad (68)$$

where the last approximate equality is valid for  $\beta_{\text{ms}} \sim 0.5$ . The scale of transition to an impulsive regime is now

$$R_{\text{cr,h}} = \frac{ct_v}{\Delta\beta_h} \sim ct_v\Gamma^2. \quad (69)$$

For the typical parameters of AGN jets, this reads

$$R_{\text{cr,h}} \sim 1 \left( \frac{t_v}{10 \text{ d}} \right) \left( \frac{\sigma_0}{10} \right)^2 \text{ pc}. \quad (70)$$

Basically, since  $\beta_{\text{ms}}$  is mildly relativistic, we have  $R_{\text{cr,h}} \sim R_{\text{cr,t}}$ , and since  $\Gamma \sim \sigma_0$  there, the two distances are also of the order of  $R_c \approx \sigma_0^2 ct_v$ . Thus, the theory predicts effective dissipation at internal shocks on the scales of  $\sim 1$ – $10$  pc, exactly the region where VLBI observations reveal bright superluminal knots of AGN jets. This is the AGN counterpart of the prompt emission region of GRBs.

## 6 SUMMARY AND CONCLUSIONS

In this paper, we investigated the properties of magnetic acceleration of relativistic impulsive flows. As a first step, we focused on a relatively simple test case where a uniformly cold and highly magnetized ( $\sigma_0 \gg 1$ ) shell of initial width  $l_0$ , whose back end leans against a conducting ‘wall’ and whose head faces vacuum, was considered. The evolution of the flow that develops in this test case splits into three distinct phases.

The first phase can be described as a formation of a plasma pulse (or a moving shell). During this phase, which lasts for the time  $\sim t_0 \equiv l_0/c_{\text{ms},0} \approx l_0/c$ , a self-similar rarefaction wave develops at the interface with vacuum and travels towards the wall. At the end of this phase, the mean Lorentz factor of the outflow is only  $\langle \Gamma \rangle \sim \sigma_0^{1/3}$  and, apart from the very thin layer at the vacuum interface, the shell of plasma is still highly magnetized, with a mean magnetization parameter of  $\langle \sigma \rangle \sim \sigma_0^{2/3}$ .

The first phase ends when the rarefaction wave reaches the wall. At this point, a secondary rarefaction wave forms that propagates from the wall into the back of the shell and decelerates the material that passes through it so that the shell quickly separates from the wall and moves away from it. During this second phase, the CM Lorentz factor of the shell remains fairly constant ( $\Gamma_{\text{CM}} \sim \sigma_0^{1/2}$ ). However, the leading part of the plasma shell, ahead of the secondary rarefaction, continues to accelerate at the same rate as in the self-similar solution. It contains most of the shell energy and its mean Lorentz factor grows as  $\langle \Gamma \rangle \propto t^{1/3}$ .

At the end of the second phase, which lasts up to  $\sim t_c \equiv \sigma_0^2 t_0$ , the magnetization of the shell drops down to  $\sigma \sim 1$ , one-half of the electromagnetic energy is converted into the bulk motion kinetic energy of the plasma, and the growth of the mean Lorentz factor begins to saturate at  $\langle \Gamma \rangle \sim \sigma_0$ . Thus, the flow enters a phase of coasting. During the coasting phase, the pulse width grows faster,

approaching  $l \propto t$ . The decrease in the magnetization parameter also accelerates, approaching  $\sigma \propto t^{-1}$ , and the pulse soon becomes kinetic-energy-dominated. This property of impulsive magnetic acceleration is most valuable in astrophysical context as the efficiency of relativistic MHD shock dissipation decreases dramatically with magnetization. In contrast to an impulsive flow, a steady-state magnetized jet either remains highly magnetized ( $\sigma \gg 1$ ) all the way or approaches  $\sigma \approx 1$ , depending on the efficiency of external collimation. This implies at best only modest shock dissipation efficiency.

In some cases of truly explosive phenomena, such as magnetar flares, our impulsive magnetic acceleration mechanism can be solely responsible for the flow acceleration. In most other cases, such as GRBs and AGN jets, strong variability of their central engines is not expected on time-scales below the viscous time-scale of the inner accretion disc around a black hole, which powers relativistic outflow. This gives plenty of time to establish a quasi-steady superfast-magnetosonic flow near the source, where it is accelerated via the collimation mechanism. The observed strong collimation of these jets supports our conclusion that the collimation mechanism plays a part in their acceleration. The impulsive acceleration mechanism comes in force farther out, where an individual ejecta element starts being accelerated after the head rarefaction crosses it and creates conditions similar to those of our test case flow in phases 2 and 3. The mean Lorentz factor of the shell, however, starts increasing significantly above the value achieved by the quasi-steady collimation acceleration only when the tail rarefaction wave crosses about half of the shell. Provided the central engine variability is sufficiently strong, so that the flow can be described as individual ejecta shells separated by long gaps, the impulsive acceleration mechanism can complete the acceleration process and produce kinetic-energy-dominated relativistic flows on astrophysically relevant distances from the central engine. For short GRBs, this may still work well even if the ejecta effectively forms a single uniform shell.

Our analysis of GRBs shows that a combination of the collimation and impulsive mechanisms can accelerate GRB jets up to  $\Gamma \gtrsim 10^3$ , as has been inferred recently for several bright GRBs detected by the Fermi Large Area Telescope, for both long (Abdo et al. 2009a,b) and short (Ackermann et al. 2010) duration GRBs.<sup>14</sup> Moreover, their jets can become kinetic-energy-dominated before the interaction with the interstellar or stellar wind gas begins to decelerate the ejecta at  $R_{\text{dec}} \sim 10^{16}$ – $10^{17}$  cm. The dissipation at internal shocks can become efficient on scales  $R \gtrsim R_c \approx 10^{13}(\sigma_0/300)^2(t_v/4 \text{ ms}) \text{ cm}$ . The large variation in the Lorentz factor at the coasting phase,  $\Delta\Gamma \sim \Gamma$ , ensures that the internal shock will be strong and can dissipate and radiate of the order of  $\sim 10$  per cent or so of the flow kinetic energy, leading to a possibility of strong prompt emission.

The AGN jets are likely to be accelerated up to their observed Lorentz factors already during the collimation acceleration phase. However, the impulsive acceleration phase remains important, providing effective conversion of the remaining electromagnetic energy and producing kinetic-energy-dominated flows. Our estimates show that an efficient shock dissipation region, analogous to the prompt emission region of GRBs, is located around  $\sim 1$ –

<sup>14</sup> We do note, however, that these lower limits on  $\Gamma$  from pair opacity are somewhat model-dependent and a fully self-consistent calculation appropriate for an internal shock origin of the gamma-ray emission gives limits that are a factor of  $\sim 3$  lower (Granot, Cohen-Tanugi & do Couto e Silva 2008; Ackermann et al. 2011),  $\Gamma \gtrsim 10^{2.5}$ , which are significantly easier to satisfy.

10 pc, where VLBI observations reveal the presence of superluminal ‘blobs’.

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## APPENDIX A: SELF-SIMILAR RAREFACTION WAVE IN PLANAR SYMMETRY

The equations of relativistic MHD can be written as

$$\partial_\mu T^{\mu\nu} = 0, \quad \partial_\mu F^{*\mu\nu} = 0, \quad \partial_\mu(\rho u^\mu) = 0, \quad (\text{A1})$$

(see Komissarov 1999, and references therein), where

$$T^{\mu\nu} = (\rho h_g + b^2) u^\mu u^\nu + \left(p_g + \frac{b^2}{2}\right) g^{\mu\nu} - b^\mu b^\nu, \quad (\text{A2})$$

is the energy momentum tensor. Here  $\rho$ ,  $w_g = \rho h_g$ ,  $p_g$  and  $u^\mu = (u^0, \mathbf{u}) = \Gamma(1, \mathbf{v})$  are the fluid proper rest-mass density, enthalpy density, pressure and four-velocity, where  $\Gamma = (1 - v^2)^{-1/2}$  is its Lorentz factor,  $g^{\mu\nu}$  is the metric tensor, and we use units where  $c = 1$  for convenience. Furthermore,

$$F^{*\mu\nu} = b^\mu u^\nu - b^\nu u^\mu \quad (\text{A3})$$

is the dual tensor of the electromagnetic field and  $b^\mu = (b^0, \mathbf{b})$ , where

$$b^0 = \mathbf{B} \cdot \mathbf{u} = \Gamma \mathbf{B} \cdot \mathbf{v}, \quad \mathbf{b} = \frac{\mathbf{B} + b^0 \mathbf{u}}{u^0} = \frac{\mathbf{B}}{\Gamma} + \Gamma(\mathbf{v} \cdot \mathbf{B}) \mathbf{v}, \quad (\text{A4})$$

is the four-vector of the magnetic field, which is defined as

$$b_\alpha = \frac{1}{2} \eta_{\alpha\beta\gamma\delta} u^\beta F^{\gamma\delta}, \quad (\text{A5})$$

where  $F^{\gamma\delta}$  is the electromagnetic tensor and  $\eta_{\alpha\beta\gamma\delta}$  is the Levi–Civita alternating tensor. In the fluid rest frame,  $b^\mu = (0, \mathbf{B})$ , where  $\mathbf{B}$  is the usual three-vector magnetic field, divided by  $\sqrt{4\pi}$ , so that  $w_m = 2p_m = b^2$ . In general,  $\mathbf{B}$  is measured in the laboratory frame. The three vectors of the magnetic and electric fields in an arbitrary frame are given by

$$\mathbf{B} = F^{*i0} = \mathbf{b}u^0 - u\mathbf{b}^0, \quad \mathbf{E} = \mathbf{b} \times \mathbf{u}. \quad (\text{A6})$$

Similar to classical MHD, the electric current is given by the second Maxwell equation,

$$J^\nu = \partial_\mu F^{\mu\nu}, \quad (\text{A7})$$

where it also includes the displacement current (time-derivatives of the electric field). Finally,  $\nabla \cdot \mathbf{B} = \partial_i F^{*i0} = 0$ ,  $u_\mu b^\mu = 0$ ,  $u_\mu u^\mu = -1$ .

The RMHD equations simplify considerably under the assumption of a flat space–time,  $g^{\mu\nu} = \eta^{\mu\nu} = \text{diag}(-1, 1, 1, 1)$ , and planar symmetry, that is, all quantities depend only on  $x$  and  $t$  in a Cartesian coordinate system (see e.g. Giacomazzo & Rezzolla 2006):

$$\frac{\partial}{\partial t} \begin{pmatrix} \rho\Gamma \\ \rho h\Gamma^2 - p - \rho\Gamma - b^0 b^0 \\ \rho h\Gamma^2 v^x - b^0 b^x \\ \rho h\Gamma^2 v^y - b^0 b^y \\ \rho h\Gamma^2 v^z - b^0 b^z \\ B^y \\ B^z \end{pmatrix} + \frac{\partial}{\partial x} \begin{pmatrix} \rho\Gamma v^x \\ \rho h\Gamma^2 v^x - b^0 b^x - \rho\Gamma v^x \\ \rho h\Gamma^2 v^x v^x + p - b^x b^x \\ \rho h\Gamma^2 v^y v^x - b^x b^y \\ \rho h\Gamma^2 v^y v^z - b^x b^z \\ B^y v^x - B^x v^y \\ B^z v^x - B^x v^z \end{pmatrix} = 0. \quad (\text{A8})$$

Here we consider the even simpler case where  $v^y = v^z = 0$  and  $B^x = B^z = 0$  so that  $\mathbf{v} = v\hat{x}$  and  $\mathbf{B} = B\hat{y}$ , that is,  $u^\mu = \Gamma(1, v, 0, 0)$  and  $b^\mu = (0, 0, B/\Gamma, 0)$ . Under these conditions, the RMHD equations further simplify to

$$\frac{\partial}{\partial t} \begin{pmatrix} \rho\Gamma \\ \rho h\Gamma^2 - p - \rho\Gamma \\ \rho h\Gamma^2 v \\ B \end{pmatrix} + \frac{\partial}{\partial x} \begin{pmatrix} \rho\Gamma v \\ \rho h\Gamma^2 v - \rho\Gamma v \\ \rho h\Gamma^2 v^2 + p \\ Bv \end{pmatrix} = 0 \quad (\text{A9})$$

and the magnetic field in the fluid rest frame is given by  $B' = B/\Gamma$ , so that the equations for the evolution of  $\rho\Gamma$  and  $B = B'\Gamma$  are the same and  $B/\rho\Gamma = B'/\rho = \text{constant}$ . Thus, we are left with three equations for three variables (e.g.  $\rho$ ,  $\Gamma$  and  $p_g$ ), where we also need to assume an equation of state. In our notation

$$h = h_g + \frac{b^2}{\rho}, \quad h_g = 1 + \epsilon + \frac{p_g}{\rho} = 1 + \frac{\gamma}{\gamma - 1} \frac{p_g}{\rho}, \quad (\text{A10})$$

where  $\epsilon = e_{\text{int}}/\rho$  and  $e_{\text{int}} = \epsilon\rho = w_g - p_g - \rho$  is the proper internal energy density of the fluid, while  $\gamma$  is the adiabatic index of the fluid. The total pressure is given by  $p = p_g + p_m = p_g + b^2/2$ .

We are looking for rarefaction wave solutions, which are self-similar, that is, all quantities depend on  $x$  and  $t$  only through their ratio, which is defined as the self-similar variable:  $\xi \equiv x/t$ . In rarefaction waves, the specific entropy,  $s$ , of every fluid element is conserved and therefore  $0 = ds/dt = \partial s/\partial t + v\partial s/\partial x$ . Since  $\partial/\partial x = (1/t)d/d\xi$  and  $\partial/\partial t = -(\xi/t)d/d\xi$ , this implies  $(v - \xi)s' = 0$ , where a prime denotes a derivative with respect to  $\xi$  ( $s' \equiv ds/d\xi$ ), and therefore  $s' = 0$  and  $s = \text{constant}$  (in general  $v \neq \xi$ ). Therefore, the flow is isentropic and we may simply relate the pressure to its value ahead of the rarefaction wave,

$$b^2 = \left(\frac{B_0}{\rho_0}\right)^2 \rho^2 = \rho_0 \sigma_0 \tilde{\rho}^2, \quad (\text{A11})$$

$$p_g = p_{g,0} \left(\frac{\rho}{\rho_0}\right)^\gamma = \rho_0 a_0 \tilde{\rho}^\gamma, \quad (\text{A12})$$

$$p = p_{g,0} \left(\frac{\rho}{\rho_0}\right)^\gamma + \frac{1}{2} \left(\frac{B_0}{\rho_0}\right)^2 \rho^2 = \rho_0 \left(a_0 \tilde{\rho}^\gamma + \frac{\sigma_0}{2} \tilde{\rho}^2\right), \quad (\text{A13})$$

$$\rho h = \rho + \frac{\gamma}{\gamma - 1} p_{g,0} \left(\frac{\rho}{\rho_0}\right)^\gamma + B_0^2 \left(\frac{\rho}{\rho_0}\right)^2 = \rho_0 \left(\tilde{\rho} + \frac{\gamma}{\gamma - 1} a_0 \tilde{\rho}^\gamma + \sigma_0 \tilde{\rho}^2\right), \quad (\text{A14})$$

where  $\tilde{\rho} \equiv \rho/\rho_0$ ,  $a_0 \equiv p_{g,0}/\rho_0$ , and  $\sigma_0 \equiv B_0^2/\rho_0$  is the magnetization parameter of the fluid ahead of the rarefaction wave (which is assumed to be at rest in the laboratory frame:  $\Gamma_0 = 1$ ).

Equation (A9) can be expressed in terms of the self-similar variable  $\xi$  as

$$0 = (v - \xi)(\rho' + \rho\Gamma^2 v v') + \rho v', \quad (\text{A15})$$

$$0 = (v - \xi)(\rho h\Gamma^2)' + \xi p' + \rho h\Gamma^2 v', \quad (\text{A16})$$

$$0 = (1 - v\xi)p' + (v - \xi)\rho h\Gamma^2 v'. \quad (\text{A17})$$

Let  $c_s$ ,  $c_A$  and  $c_{ms}$  denote the sound speed, the Alfven speed and the fast-magnetosonic speed, respectively. We have  $c_s^2 = (1/h_g)(\partial p_g/\partial \rho)_s$  and  $c_A^2 = b^2/\rho h$ , so that  $h_g/h = 1 - c_A^2$  and

$$c_{ms}^2 = \frac{1}{h} \left( \frac{\partial p}{\partial \rho} \right)_s = c_A^2 + c_s^2 (1 - c_A^2), \quad (\text{A18})$$

which implies  $p' = c_{ms}^2 h \rho'$ . Therefore, equation (A17) can be rewritten as

$$0 = (1 - v\xi)c_{ms}^2 \rho' + (v - \xi)\rho \Gamma^2 v'. \quad (\text{A19})$$

Equations (A15) and (A19) imply  $c_{ms}^2 = [(v - \xi)/(1 - v\xi)]^2$  and therefore

$$c_{ms} = \pm \frac{v - \xi}{1 - v\xi}, \quad (\text{A20})$$

where the plus and minus signs correspond to rarefaction waves propagating to the left-hand and right-hand sides, respectively. This also implies

$$\xi = \frac{v \mp c_{ms}}{1 \mp v c_{ms}}. \quad (\text{A21})$$

The velocities of the tail (where  $v = 0$ ) and of the head (where  $c_{ms} = 0$ ) of the rarefaction wave are given by

$$\xi_t = \mp c_{ms} \quad \text{and} \quad \xi_h = \pm v_{\max}, \quad (\text{A22})$$

respectively, where  $v_{\max} = \max |v|$  is obtained at the head of the rarefaction wave. As expected, the tail of the rarefaction wave propagates into the fluid at rest at the fast-magnetosonic speed.

Equations (A19) and (A20) imply

$$\Gamma^2 dv \pm \frac{c_{ms}}{\rho} d\rho = 0 \implies J_{\pm} = \frac{1}{2} \ln \left( \frac{1+v}{1-v} \right) \pm \int_0^{\tilde{\rho}} \frac{c_{ms}(\tilde{\rho}')}{\tilde{\rho}'} d\tilde{\rho}' = \text{constant}. \quad (\text{A23})$$

Under our assumptions,

$$c_{ms}(\tilde{\rho}) = \sqrt{\frac{\gamma a_0 \tilde{\rho}^{\gamma-1} + \sigma_0 \tilde{\rho}}{1 + [\gamma/(\gamma-1)] a_0 \tilde{\rho}^{\gamma-1} + \sigma_0 \tilde{\rho}}}, \quad (\text{A24})$$

so that the integral in equation (A23) can be calculated analytically in the simple cases, where  $\sigma_0 = 0$  ( $B_0 = 0$ ) or  $a_0 = 0$  ( $p_{g,0} = 0$ ). In the first limit ( $\sigma_0 = 0$  i.e. no magnetic field),

$$J_{\pm} = \frac{1}{2} \ln \left( \frac{1+v}{1-v} \right) \pm \frac{1}{\sqrt{\gamma-1}} \ln \left( \frac{\sqrt{\gamma-1} + c_s}{\sqrt{\gamma-1} - c_s} \right) = \text{constant}, \quad (\text{A25})$$

(Marti & Müller 1994), so that

$$\left( \frac{1+v}{1-v} \right) \left( \frac{\sqrt{\gamma-1} + c_s}{\sqrt{\gamma-1} - c_s} \right)^{\pm \frac{2}{\sqrt{\gamma-1}}} = \text{constant}, \quad (\text{A26})$$

and in the limit  $a_0 \gg 1$  and  $\gamma = 4/3$ , this implies  $\Gamma_{\max} \gg 1$ , which is approximately given by

$$\Gamma_{\max} \approx \frac{1}{2} \left[ \frac{4\gamma a_0}{(\gamma-1)} \right]^{(\gamma-1)^{-1/2}} = \begin{cases} 2^{4\sqrt{3}-1} a_0^{\sqrt{3}} & (\gamma = 4/3), \\ 4a_0 = 4p_{g,0}/\rho_0 & (\gamma = 2). \end{cases} \quad (\text{A27})$$

In the second limit ( $a_0 = 0$ ), we find

$$J_{\pm} = \frac{1}{2} \ln \left( \frac{1+v}{1-v} \right) \pm 2 \text{ArcSinh}(\sqrt{\sigma_0 \tilde{\rho}}) = \frac{1}{2} \ln \left( \frac{1+v}{1-v} \right) \pm 2 \ln \left( \sqrt{\sigma_0 \tilde{\rho}} + \sqrt{\sigma_0 \tilde{\rho} + 1} \right) = \text{constant}, \quad (\text{A28})$$

so that

$$\left( \frac{1+v}{1-v} \right) \left( \sqrt{\sigma_0 \tilde{\rho}} + \sqrt{\sigma_0 \tilde{\rho} + 1} \right)^{\pm 4} = \text{constant}, \quad (\text{A29})$$

and in the limit  $\sigma_0 \gg 1$ , we have

$$\Gamma_{\max} \approx 2\sigma_0. \quad (\text{A30})$$

It can be seen that the purely magnetic case,  $a_0 = 0$ , is equivalent to the pure hydrodynamic case,  $\sigma_0 = 0$ , for  $\gamma = 2$  and  $a_0 \rightarrow \sigma_0/2$ . In the more general case,

$$J_{\pm} = \frac{1}{2} \ln \left( \frac{1+v}{1-v} \right) \pm I(\tilde{\rho}) = \pm I(1) = \text{constant}, \quad (\text{A31})$$

where

$$I(\tilde{\rho}) = \int_0^{\tilde{\rho}} \frac{d\tilde{\rho}}{\tilde{\rho}} \sqrt{\frac{\gamma a_0 \tilde{\rho}^{\gamma-1} + \sigma_0 \tilde{\rho}}{1 + [\gamma/(\gamma-1)] a_0 \tilde{\rho}^{\gamma-1} + \sigma_0 \tilde{\rho}}}, \quad (\text{A32})$$

so that

$$v_{\max} = \frac{\exp[2I(1)] - 1}{\exp[2I(1)] + 1}, \quad \Gamma_{\max} = \frac{\exp[I(1)]}{1 + v_{\max}} = \frac{\exp[2I(1)] + 1}{2 \exp[I(1)]} \quad (\text{A33})$$

and

$$v = \pm \frac{\exp[2\tilde{I}(\tilde{\rho})] - 1}{\exp[2\tilde{I}(\tilde{\rho})] + 1}, \quad \Gamma = \frac{\exp[2\tilde{I}(\tilde{\rho})] + 1}{2 \exp[\tilde{I}(\tilde{\rho})]}, \quad (\text{A34})$$

where

$$\tilde{I}(\tilde{\rho}) = I(1) - I(\tilde{\rho}) = \int_{\tilde{\rho}}^1 \frac{d\tilde{\rho}}{\tilde{\rho}} \sqrt{\frac{\gamma a_0 \tilde{\rho}^{\gamma-1} + \sigma_0 \tilde{\rho}}{1 + [\gamma/(\gamma-1)] a_0 \tilde{\rho}^{\gamma-1} + \sigma_0 \tilde{\rho}}}. \quad (\text{A35})$$

## APPENDIX B: THE AVERAGE LORENTZ FACTOR

The maximal Lorentz factor,  $\Gamma_{\max}$ , is only asymptotically reached at the very head of the rarefaction wave and only a small amount of material, which carries a small fraction of the total energy, has  $\Gamma \sim \Gamma_{\max}$ . Therefore, it makes sense to calculate some average value of the Lorentz factor, which would reflect better the Lorentz factor of the material that carries most of the energy. A natural definition is the weighted average over the energy:

$$\langle \Gamma \rangle_E \equiv \frac{\int \Gamma dE}{\int dE} = \frac{\int dx T^{00} \Gamma}{\int dx T^{00}} = \frac{\int_{\xi_t}^{\xi_h} d\xi T^{00} \Gamma}{\int_{\xi_t}^{\xi_h} d\xi T^{00}}, \quad (\text{B1})$$

where

$$T^{00} = \rho_0 \left[ \Gamma^2 \left( \tilde{\rho} + \frac{\gamma}{\gamma-1} a_0 \tilde{\rho}^\gamma + \sigma_0 \tilde{\rho}^2 \right) - a_0 \tilde{\rho}^\gamma - \frac{\sigma_0}{2} \tilde{\rho}^2 \right]. \quad (\text{B2})$$

Another possible definition is the weighted average over the rest mass:

$$\langle \Gamma \rangle_M \equiv \frac{\int \Gamma dM}{\int dM} = \frac{\int dx \Gamma^2 \rho}{\int dx \Gamma \rho} = \frac{\int_{\xi_t}^{\xi_h} d\xi \Gamma^2 \rho}{\int_{\xi_t}^{\xi_h} d\xi \Gamma \rho}. \quad (\text{B3})$$

We note that for a cold magnetized shell, at late times when almost all of the energy is in kinetic form and the magnetic energy becomes negligible, the numerator approaches  $E/c^2$ , and since the denominator is simply the rest mass  $M$ ,  $\langle \Gamma \rangle_M$  approaches  $E/Mc^2 = 1 + \sigma_0/2$ . Alternative options to define a ‘typical’ Lorentz factor are its average over space

$$\langle \Gamma \rangle_x \equiv \frac{\int dx \Gamma}{\int dx} = \frac{\int_{\xi_t}^{\xi_h} d\xi \Gamma}{\int_{\xi_t}^{\xi_h} d\xi}, \quad (\text{B4})$$

or its value at the point where there are equal energies on either side within the rarefaction wave in the laboratory frame (i.e. the ‘energy median’ value):

$$\langle \Gamma \rangle_{E,\text{med}} \equiv \left\{ \Gamma(x_{1/2}) \left| \int_{x_{\min}}^{x_{1/2}} dx T^{00} = \int_{x_{1/2}}^{x_{\max}} dx T^{00} \right. \right\} = \left\{ \Gamma(\xi_{1/2}) \left| \int_{\xi_t}^{\xi_{1/2}} d\xi T^{00} = \int_{\xi_{1/2}}^{\xi_h} d\xi T^{00} \right. \right\}, \quad (\text{B5})$$

where  $x_{\min} = t\xi_t$  and  $x_{\max} = t\xi_h$  (see equation A22).

Fig. B1 shows these three estimates for the typical Lorentz factor within the rarefaction wave, for the pure hydrodynamic case ( $\sigma_0 = 0$ ; left-hand panel) and for the pure magnetic case ( $a_0 = 0$ ; right-hand panel). In the pure hydrodynamics case, the typical Lorentz factor of the material in the rarefaction wave is only mildly relativistic even in the limit of  $a_0 \gg 1$ , where it approaches a constant value, while  $\Gamma_{\max}$  rapidly increases with  $a_0$  (see equation A27). In the purely magnetic case, we find that the typical value of the Lorentz factor within the rarefaction wave is  $\langle \Gamma \rangle \approx \sigma_0^{1/3}$ , while its maximal value at the head of the rarefaction wave is  $\Gamma_{\max} \approx 2\sigma_0$ .

## APPENDIX C: ANALYTIC DERIVATIONS FOR THE RAREFACTION WAVES

### C1 Explicit solution for the original self-similar rarefaction wave

Equation (5) can be rewritten as

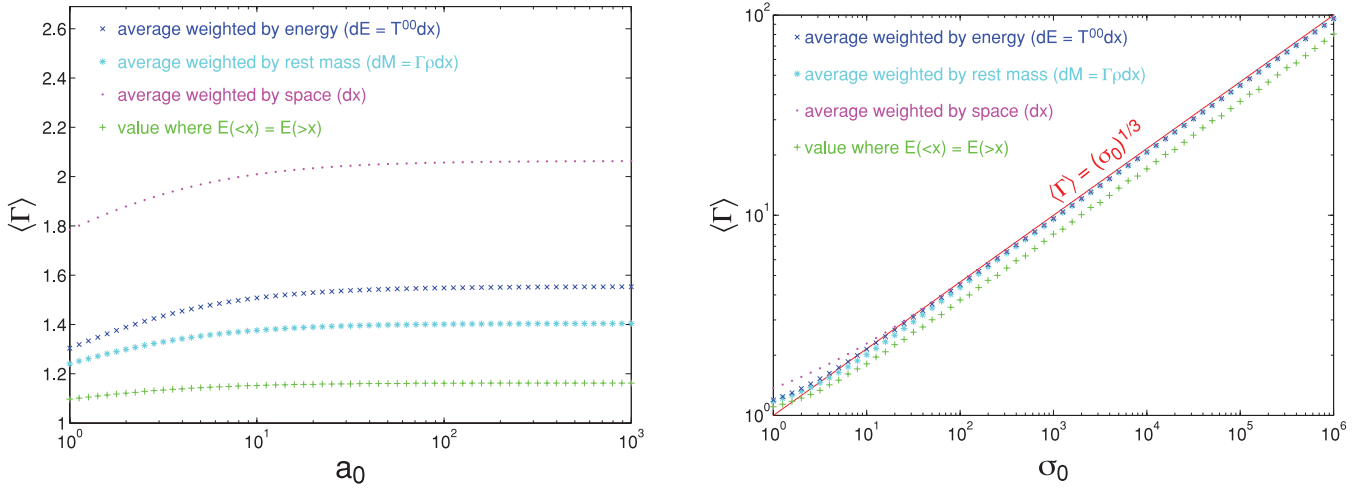
$$\delta_\xi^2 = \delta_v^2 \delta_{\text{cms}}^{-2}, \quad (\text{C1})$$

and equation (6) can be rewritten as

$$\delta_v^2 \delta_{\text{cms}}^4 = \delta_{\text{cms},0}^4 = \mathcal{J}_+ = \left( \sqrt{\sigma_0} + \sqrt{\sigma_0 + 1} \right)^4, \quad (\text{C2})$$

where  $\delta_X$  is defined via

$$\delta_X^2 = \frac{1+X}{1-X}, \quad X = \frac{\delta_X^2 - 1}{\delta_X^2 + 1}.$$



**Figure B1.** Left-hand panel: four different estimates for the ‘typical’ Lorentz factor,  $\langle \Gamma \rangle$ , within a rarefaction wave for the pure hydrodynamic case ( $\sigma_0 = 0$ ) and for an adiabatic index of  $\gamma = 4/3$ , as a function of  $a_0 = p_0/\rho_0 c^2$ . Various symbols show different weightings of  $\Gamma$ . Right-hand panel: the same four estimates of the ‘typical’ Lorentz factor within the rarefaction wave for the pure magnetic case ( $a_0 = 0$ ), as a function of  $\sigma_0$ . The red solid line corresponding to  $\langle \Gamma \rangle = \sigma_0^{1/3}$  has been added for reference.

This allows us to find all flow variables as explicit functions of  $\xi$ :

$$\delta_v = (\delta_{\text{cms},0} \delta_\xi)^{2/3}, \quad v = \frac{(\delta_{\text{cms},0} \delta_\xi)^{4/3} - 1}{(\delta_{\text{cms},0} \delta_\xi)^{4/3} + 1}, \quad \Gamma = \frac{(\delta_{\text{cms},0} \delta_\xi)^{4/3} + 1}{2 (\delta_{\text{cms},0} \delta_\xi)^{2/3}}, \quad u = \Gamma v = \frac{(\delta_{\text{cms},0} \delta_\xi)^{4/3} - 1}{2 (\delta_{\text{cms},0} \delta_\xi)^{2/3}}, \quad (\text{C3})$$

$$\delta_{\text{cms}} = \frac{\delta_{\text{cms},0}^{2/3}}{\delta_\xi^{1/3}}, \quad c_{\text{ms}}^2 = \frac{\sigma}{1 + \sigma} = \left[ \frac{\delta_{\text{cms},0}^{4/3} \delta_\xi^{-2/3} - 1}{\delta_{\text{cms},0}^{4/3} \delta_\xi^{-2/3} + 1} \right]^2, \quad (\text{C4})$$

$$\frac{\sigma}{\sigma_0} = \frac{\rho}{\rho_0} = \frac{B'}{B_0} = \frac{B}{\Gamma B_0} = \frac{1}{4\sigma_0} \left( \frac{\delta_{\text{cms},0}^{2/3}}{\delta_\xi^{1/3}} - \frac{\delta_\xi^{1/3}}{\delta_{\text{cms},0}^{2/3}} \right)^2, \quad (\text{C5})$$

(this result is due to Lyutikov 2010a, with a small correction in equation C5). The extent of the rarefaction wave is given by the conditions  $\delta_{\text{cms}} = 1$  for the right-hand front and  $\delta_v = 1$  for the left-hand front. They yield  $\delta_{\text{cms},0}^{-1} \leq \delta_\xi \leq \delta_{\text{cms},0}^2$ .

## C2 Motion of the head of the secondary rarefaction wave

The overall impression created by Fig. 2 is that of an effective separation of the shell from the wall. The region between  $x = 18l_0$  and  $20l_0$  contains most of the total mass and energy of the initial solution. This somewhat surprising result can be verified in a different way. In the fluid frame, the front of secondary rarefaction moves with the local magnetosonic speed. In the laboratory frame, this corresponds to

$$\beta_* \equiv \frac{dx_*}{dt} = \frac{v(\xi_*) + c_{\text{ms}}(\xi_*)}{1 + v(\xi_*)c_{\text{ms}}(\xi_*)} = \frac{\delta_{\text{cms},0}^{8/3} \delta_{\xi_*}^{2/3} - 1}{\delta_{\text{cms},0}^{8/3} \delta_{\xi_*}^{2/3} + 1}, \quad (\text{C6})$$

where  $v(\xi)$  and  $c_{\text{ms}}(\xi)$  describe the self-similar solution for the initial rarefaction (equations C3 and C4). Noting that  $d\xi_*/dt = [(dx_*/dt) - \xi_*]/t$  and  $d\delta_{\xi_*}^2/dt = (d\delta_{\xi_*}^2/d\xi_*)(d\xi_*/dt) = (d\xi_*/dt)(\delta_{\xi_*}^2 + 1)^2/2$ , equation (C6) can be rewritten as

$$\frac{d\delta_{\xi_*}^2}{d \ln t} = \delta_{\xi_*}^2 + 1 - \frac{(\delta_{\xi_*}^2 + 1)^2}{\delta_{\text{cms},0}^{8/3} (\delta_{\xi_*}^2)^{1/3} + 1}, \quad (\text{C7})$$

which has the solution (Lyutikov 2010a):

$$\frac{t}{t_{0,*}} = (\delta_{\xi_*}^2 + 1) \left[ 1 - \left( \frac{\delta_{\xi_*}^2}{\delta_{\text{cms},0}^4} \right)^{2/3} \right]^{-3/2}, \quad (\text{C8})$$

where  $\delta_{\xi_*} < \delta_{\text{cms},0}^2$  and

$$\frac{t_{0,*}}{t_0} = \frac{(\delta_{\text{cms},0}^4 - 1)^{3/2}}{\delta_{\text{cms},0}^4 (\delta_{\text{cms},0}^2 + 1)} = \frac{4\sigma_0^{3/4}(1 + \sigma_0)^{1/4}}{(\sqrt{1 + \sigma_0} + \sqrt{\sigma_0})^2}. \quad (\text{C9})$$

For  $\sigma_0 \gg 1$ , we find that  $t_{0,*} \approx t_0$ , so that at  $t \gg t_0$ , we have  $\delta_{\xi_*}^2 \approx 2/(1 - \xi_*) \gg 1$  and

$$\frac{t}{t_0} \approx \frac{2}{1 - \xi_*} \left[ 1 - \frac{1}{4\sigma_0^{4/3}(1 - \xi_*)^{2/3}} \right]^{-3/2}, \quad 1 - \xi_* \approx \frac{1}{8\sigma_0^2} \left[ 1 + \left( \frac{t}{16\sigma_0^2 t_0} \right)^{-2/3} \right]^{3/2} \approx \begin{cases} 2t_0/t & t \ll 16\sigma_0^2 t_0, \\ 1/8\sigma_0^2 & t \gg 16\sigma_0^2 t_0, \end{cases} \quad (\text{C10})$$

For  $\sigma_0 \gg 1$ , we also have  $\delta_{\text{cms},0}^2 \approx 4\sigma_0$ , so that for  $t_0 \ll t \ll 16\sigma_0^2 t_0$ , where  $\delta_{\xi_*}^2 \approx t/t_0$ , equations (C3) and (10) imply

$$\Gamma(\xi_*) \approx \left( \frac{\sigma_0 t}{2t_0} \right)^{1/3}, \quad \Gamma_* = (1 - \beta_*^2)^{-1/2} \approx \left( \frac{4\sigma_0^4 t}{t_0} \right)^{1/6}. \quad (\text{C11})$$

Note that  $\Gamma_*$  is the Lorentz factor of the motion of the head of the secondary rarefaction wave, while  $\Gamma(\xi_*)$  is the Lorentz factor of the fluid at that location.

### C3 Analytic calculation of physical quantities at $\xi > \xi_*(t)$

It is instructive to calculate the values of relevant physical quantities in the region between the head of the secondary rarefaction wave and the vacuum interface, which corresponds to  $\xi_*(t) < \xi < \beta_{\text{max}}$ . In particular, it can help verify that this region contains most of the energy and rest mass in the flow during the magnetic rocket acceleration phase (at  $t \ll t_c = \sigma_0^2 t_0$ ). Using equations (C3) and (C5), at a given time  $t$ , we have  $dx = t d\xi$ , so that the rest mass per unit area at  $\xi > \xi_*$  is given by

$$M[> \xi_*(t)] = \int_{x_*(t)}^{x_{\text{vac}}(t)} dx \Gamma(x) \rho(x) = \frac{\rho_0 t}{8\sigma_0} \int_{\xi_*(t)}^{\beta_{\text{max}}} d\xi \left( \delta_{\text{cms},0}^{2/3} \delta_{\xi}^{2/3} + \frac{1}{\delta_{\text{cms},0}^{2/3} \delta_{\xi}^{2/3}} \right) \left( \frac{\delta_{\text{cms},0}^{2/3}}{\delta_{\xi}^{1/3}} - \frac{\delta_{\xi}^{1/3}}{\delta_{\text{cms},0}^{2/3}} \right)^2, \quad (\text{C12})$$

where

$$\beta_{\text{max}} = \frac{2\sqrt{\sigma_0(1 + \sigma_0)}}{1 + 2\sigma_0} \quad (\text{C13})$$

is the maximal fluid velocity, which is obtained at the vacuum interface, while  $\xi_*(t)$  is given implicitly by equation (C8). One can change variables of integration to  $\delta_{\xi}^2$  and then to  $y = \delta_{\xi}^{2/3}$ , using the relations

$$d\xi = \frac{2d\delta_{\xi}^2}{(\delta_{\xi}^2 + 1)^2} = \frac{6y^2 dy}{(y^3 + 1)^2}, \quad (\text{C14})$$

and use the simple expression for the initial mass,  $M_0 = \rho_0 l_0 = \rho_0 t_0 [\sigma_0/(1 + \sigma_0)]^{1/2}$ , to obtain the following expression for the fraction of the initial rest mass at  $\xi > \xi_*(t)$ :

$$\frac{M[> \xi_*(t)]}{M_0} = \frac{3\sqrt{1 + \sigma_0}}{4\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) \int_{y_{\text{min}}(t)}^{a^2} dy \frac{y^2}{(y^3 + 1)^2} \left( ay + \frac{1}{ay} \right) \left( \frac{a^2}{y} - 2 + \frac{y}{a^2} \right) = \frac{\sqrt{1 + \sigma_0}}{4\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) \frac{(a^2 - y_{\text{min}})^3}{a^3(y_{\text{min}}^3 + 1)}, \quad (\text{C15})$$

where  $y_{\text{min}}(t) = \delta_{\xi_*(t)}^{2/3}$  and  $a = \delta_{\text{cms},0}^{2/3}$ . This result can be written more explicitly and simplified using equations (C8) and (C9):

$$\frac{M[> \xi_*(t)]}{M_0} = \frac{4(1 + \sigma_0)}{(\sqrt{1 + \sigma_0} + \sqrt{\sigma_0})^2} \left[ 1 + \left( \frac{\delta_{\xi_*(t)}^2}{\delta_{\text{cms},0}^2} \right)^{1/3} \right]^{-3} (\delta_{\xi_*(t)}^2 + 1) \left( \frac{t_0}{t} \right) \approx \begin{cases} 1 & t \ll \sigma_0^2 t_0, \\ 2\sigma_0^2 t_0/t & t \gg \sigma_0^2 t_0, \end{cases} \quad (\text{C16})$$

where the last asymptotic values are valid for  $\sigma_0 \gg 1$ .

Using equation (C10), one can calculate the fractional change in the width of the region between the secondary rarefaction wave and the vacuum rarefaction,  $\Delta_*(t) = t[\xi_h - \xi_*(t)]$ , where  $\xi_h = \beta_{\text{max}}$ ,

$$\frac{\Delta_*(t)}{\Delta_*(t_0)} = \frac{t[\xi_h - \xi_*(t)]}{t_0[\xi_h - \xi_i]} \approx \left[ 1 + \left( \frac{t}{16\sigma_0^2 t_0} \right)^{2/3} \right]^{3/2} - \frac{t}{16\sigma_0^2 t_0} \approx \begin{cases} 1 + (3/2)(t/16\sigma_0^2 t_0)^{2/3} & t \ll 16\sigma_0^2 t_0, \\ (3/2)(t/16\sigma_0^2 t_0)^{1/3} & t \gg 16\sigma_0^2 t_0, \end{cases} \quad (\text{C17})$$

where  $\xi_i = -c_{\text{ms},0} = -[\sigma_0/(1 + \sigma_0)]^{1/2}$ ,  $\Delta_*(t_0) = t_0 c_{\text{ms},0} \frac{3+4\sigma_0}{1+2\sigma_0} \approx 2t_0$ , and the asymptotic values are valid for  $\sigma_0 \gg 1$ .

The kinetic energy,  $E_{\text{kin}} = \int dx \Gamma(\Gamma - 1)\rho$ , is given by

$$\begin{aligned} \frac{E_{\text{kin}}[> \xi_*(t)]}{M_0} &= \frac{3\sqrt{1 + \sigma_0}}{8\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) \int_{y_{\text{min}}(t)}^{a^2} dy \frac{y^2}{(y^3 + 1)^2} \left( ay + \frac{1}{ay} \right) \left( ay + \frac{1}{ay} - 2 \right) \left( \frac{a^2}{y} - 2 + \frac{y}{a^2} \right) \\ &= \frac{\sqrt{1 + \sigma_0}}{8\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) [f(a^2) - f(y_{\text{min}}(t))], \end{aligned} \quad (\text{C18})$$

$$\begin{aligned} f(y) &= \frac{2a + 6a^4 + 2a^7 - (4a^2 + 6a^5 + a^8)y + (1 + 6a^3 + 4a^6)y^2}{a^4(1 + y^3)} \\ &\quad + \frac{1 - 2a^2 - 2a^6 + a^8}{\sqrt{3}a^4} \arctan\left(\frac{2y - 1}{\sqrt{3}}\right) + 3 \ln(y) + \frac{(a^2 + 1)^3(a^2 - 1)}{3a^4} \ln\left(\frac{1 + y}{\sqrt{1 + y^2 - y}}\right). \end{aligned} \quad (\text{C19})$$

The electromagnetic energy,  $E_{\text{EM}} = \int dx \rho_0 \sigma_0 (\Gamma^2 - \frac{1}{2})(\rho/\rho_0)^2$ , can be calculated in a similar way:

$$\begin{aligned} \frac{E_{\text{EM}}[> \xi_*(t)]}{E_{\text{EM},0}} &= \frac{2}{\sigma_0} \frac{E_{\text{EM}}[> \xi_*(t)]}{M_0} = \frac{3\sqrt{1+\sigma_0}}{16\sigma_0^{5/2}} \left( \frac{t}{t_0} \right) \int_{y_{\min}(t)}^{a^2} dy \frac{y^2}{(y^3+1)^2} \left( a^2 y^2 + \frac{1}{a^2 y^2} \right) \left( \frac{a^2}{y} - 2 + \frac{y}{a^2} \right)^2 \\ &= \frac{3\sqrt{1+\sigma_0}}{16\sigma_0^{5/2}} \left( \frac{t}{t_0} \right) [g(a^2) - g(y_{\min}(t))] , \end{aligned} \quad (\text{C20})$$

$$\begin{aligned} g(y) &= \frac{y}{a^2} - \frac{a^2}{y} - \frac{1+8a^6+a^{12}-7a^4y-4a^{10}y+4a^2y^2+7a^8y^2}{3a^6(1+y^3)} \\ &\quad - \frac{4(1-2a^2-2a^6+a^8)}{3^{3/2}a^4} \arctan\left(\frac{2y-1}{\sqrt{3}}\right) - 4\ln(y) - \frac{4(a^2+1)^3(a^2-1)}{9a^4} \ln\left(\frac{1+y}{\sqrt{1+y^2-y}}\right) . \end{aligned} \quad (\text{C21})$$

The total energy (including rest energy) is simply  $\int T^{00} dx = M + E_{\text{kin}} + E_{\text{EM}}$ . This can be used for the normalization when calculating the average values of quantities weighed by

$$T^{00}(y, a) = \frac{\rho_0}{64\sigma_0} \left[ 4 \left( ay + \frac{1}{ay} \right)^2 \left( \frac{a^2}{y} - 2 + \frac{y}{a^2} \right) + \left( a^2 y^2 + \frac{1}{a^2 y^2} \right) \left( \frac{a^2}{y} - 2 + \frac{y}{a^2} \right)^2 \right] . \quad (\text{C22})$$

We find that

$$\frac{E[> \xi_*(t)]}{E_0} = \frac{2E[> \xi_*(t)]}{(2+\sigma_0)M_0} = \frac{\sqrt{1+\sigma_0}}{16(2+\sigma_0)\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) \frac{(a^2 - y_{\min})^3 [y_{\min}(1+a^6) + 3a^2(1+a^2y_{\min}^2)]}{a^6 y_{\min} (y_{\min}^3 + 1)} \quad (\text{C23})$$

and the same holds for the energy above some  $\xi > \xi_*(t)$ , where  $y_{\min}(t) = \delta_{\xi_*(t)}^{2/3}$  is replaced by  $y(t) = \delta_{\xi}^{2/3}$ . In order to calculate the mean Lorentz  $\Gamma$  factor or magnetization  $\sigma$  at  $\xi > \xi_*$  (denoted by  $\langle \Gamma \rangle_*$  and  $\langle \sigma \rangle_*$ , respectively), one needs to calculate the following integrals:

$$\frac{1}{M_0} \int_{x_*(t)}^{x_{\text{vac}}(t)} dx T^{00} \Gamma = \frac{\sqrt{1+\sigma_0}}{\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) [f_{\Gamma}(a^2) - f_{\Gamma}(y_{\min}(t))] , \quad (\text{C24})$$

$$\begin{aligned} f_{\Gamma}(y) &= -\frac{3(a^2 - y^4)}{128a^2y^2} - \frac{9a^4(1+a^6) + a^2(1-25a^6+a^{12})y - (1-25a^6+a^{12})y^2}{64a^7(1+y^3)} - \frac{3(a^6-1)}{64a^3} \ln(1+y^3) + \frac{3(a^6-2)}{64a^3} \ln(y) \\ &\quad + \frac{(1+a^2)(1-7a^6+a^{12})}{64\sqrt{3}a^7} \arctan\left(\frac{2y-1}{\sqrt{3}}\right) + \frac{(a^2-1)(1-7a^6+a^{12})}{192a^7} \ln\left(\frac{1+y}{\sqrt{1+y^2-y}}\right) . \end{aligned} \quad (\text{C25})$$

$$\frac{1}{M_0} \int_{x_*(t)}^{x_{\text{vac}}(t)} dx T^{00} \sigma = \frac{\sqrt{1+\sigma_0}}{\sigma_0^{3/2}} \left( \frac{t}{t_0} \right) [f_{\sigma}(a^2) - f_{\sigma}(y_{\min}(t))] , \quad (\text{C26})$$

$$\begin{aligned} f_{\sigma}(y) &= -\frac{3(a^8 - 4a^6y + 4a^2y^3 - y^4)}{256a^4y^2} + \frac{2a^2(1-25a^6+a^{12}) - (1-34a^6-8a^{12})y - a^4(8+34a^6-a^{12})y^2}{128a^8(1+y^3)} - \frac{3}{128} \ln(y) \\ &\quad + \frac{1+10a^4-16a^6-16a^{10}+10a^{12}+a^{16}}{128\sqrt{3}a^8} \arctan\left(\frac{2y-1}{\sqrt{3}}\right) + \frac{(a^2+1)^5(1-5a^2+5a^4-a^6)}{384a^8} \ln\left(\frac{1+y}{\sqrt{1+y^2-y}}\right) . \end{aligned} \quad (\text{C27})$$

## APPENDIX D: GENERALIZING TO A SPHERICAL FLOW

Here we consider the case of cold ( $p_g = 0$ ) radial flow. We assume that the flow is one-dimensional and the magnetic field is perpendicular to the radial direction. Obviously, this is not fully self-consistent, but this is a reasonable approximation for an equatorial wedge. More accurate two-dimensional treatments are saved for future works.

The basic equations for a one-dimensional flow in spherical symmetry are

$$\partial_r(\rho\Gamma) + \frac{1}{r^2} \partial_r(r^2 \rho \Gamma v) = 0 \quad (\text{continuity}), \quad (\text{D1})$$

$$\partial_r(b\Gamma) + \frac{1}{r} \partial_r(rb\Gamma v) = 0 \quad (\text{magnetic field}), \quad (\text{D2})$$

$$\partial_t \left[ (\rho + b^2)\Gamma^2 - \frac{b^2}{2} \right] + \frac{1}{r^2} \partial_r [r^2(\rho + b^2)\Gamma^2 v] = 0 \quad (\text{energy}), \quad (\text{D3})$$

$$\partial_t [(\rho + b^2)\Gamma^2 v] + \frac{1}{r^2} \partial_r \left[ r^2 \left( (\rho + b^2)\Gamma^2 v^2 + \frac{b^2}{2} \right) \right] = 0 \quad (\text{momentum}), \quad (\text{D4})$$



where  $v$  is the velocity,  $b = B/\sqrt{4\pi}\Gamma$  and  $B$  is the (azimuthal) magnetic field as measured in the source frame.

One can introduce new variables,  $\bar{b}$ ,  $\bar{\rho}$  and  $x$  as follows:

$$\rho = r^{-2}\bar{\rho}, \quad b = r^{-1}\bar{b}, \quad x = r, \quad (D5)$$

which upon substitution into equations (D1)–(D3) yields

$$\partial_t(\bar{\rho}\Gamma) + \partial_x(\bar{\rho}\Gamma v) = 0, \quad (D6)$$

$$\partial_t(\bar{b}\Gamma) + \partial_x(\bar{b}\Gamma v) = 0, \quad (D7)$$

$$\partial_t \left[ (\bar{\rho} + \bar{b}^2)\Gamma^2 - \frac{\bar{b}^2}{2} \right] + \partial_x [(\bar{\rho} + \bar{b}^2)\Gamma^2 v] = 0, \quad (D8)$$

$$\partial_t [(\bar{\rho} + \bar{b}^2)\Gamma^2 v] + \partial_x \left[ \left( (\bar{\rho} + \bar{b}^2)\Gamma^2 v^2 + \frac{\bar{b}^2}{2} \right) \right] = 0. \quad (D9)$$

These equations are identical to those of plane cold ( $p_g = 0$ ) flow. Therefore, all the results obtained for the planar case, including the self-similar solution, can be utilized in the spherical case.

After the substitution  $\bar{p} \rightarrow \bar{b}^2/2$ , equations (D6), (D8) and (D9) also become identical to those of unmagnetized plasma. From equations (D6) and (D7), it follows that  $\bar{b}/\bar{\rho} = \text{constant}$ , and  $\bar{p} \propto \bar{\rho}^2$ . Thus, the ratio of specific heats for this plasma is  $\gamma = 2$ .

## APPENDIX E: SELF-SIMILAR SOLUTION FOR THE SHELL'S TAIL

Our starting point is equations (D6)–(D9), which are valid for both the planar and spherical (after making the substitutions given in equation D5) cases. Equations (D6) and (D7) imply

$$\frac{d}{dt} \left( \frac{\bar{b}}{\bar{\rho}} \right) = 0, \quad (E1)$$

that is,  $\bar{b}/\bar{\rho}$  remains constant for each fluid element and is determined by the initial conditions.

Just like in Appendix A we introduce the self-similar variable  $\xi = x/t$ , but this time we seek solutions of the form

$$v = V(\xi), \quad \bar{\rho} = t^\alpha F(\xi), \quad \bar{b} = t^\alpha G(\xi). \quad (E2)$$

(Since  $\bar{b}/\bar{\rho}$  remains constant for each fluid element,  $\bar{b}$  and  $\bar{\rho}$  must have the same temporal scaling.) Using equations (D6) and (D7), equation (D9) can be reduced to

$$\bar{\rho}\Gamma \left( \frac{\partial \Gamma v}{\partial t} + v \frac{\partial \Gamma v}{\partial x} \right) + \bar{b}^2 \Gamma^2 \frac{\partial v}{\partial t} + \frac{1}{2} \frac{\partial \bar{b}^2}{\partial x} = 0. \quad (E3)$$

Substituting the expressions (E2) into equation (E3), we obtain

$$t^\alpha F \Gamma (V - \xi)(\Gamma V)' + t^{2\alpha} (G G' - G^2 \Gamma^2 \xi V') = 0. \quad (E4)$$

This equation is satisfied for any  $t$  only in the following two cases. First, if  $\alpha = 0$  – this is the case of simple rarefaction wave analysed in Appendix A. Secondly, if

$$V = \xi \quad (E5)$$

and

$$G G' - G^2 \Gamma^2 \xi V' = 0. \quad (E6)$$

Integrating equation E6 (after substitution of equation E5 into it), we find that

$$G(\xi) = \frac{A}{\sqrt{1 - \xi^2}} = A \Gamma(\xi). \quad (E7)$$

Substituting expressions (E2) into equations (D6) and (D7) leads to

$$(1 + \alpha)F = 0, \quad (1 + \alpha)G = 0, \quad (E8)$$

which are satisfied when  $\alpha = -1$ . Function  $F(\xi)$ , however, remains undefined.

If the initial solution is uniform, as in the planar case considered in Section 2, with  $\rho_0$  and  $b_0$  being the initial rest mass density and magnetic field, respectively, then from equation (E1), we obtain

$$\bar{\rho} = \frac{\bar{\rho}_0}{\bar{b}_0} \bar{b}, \quad (E9)$$

and thus

$$F(\xi) = \frac{\bar{\rho}_0}{\bar{b}_0} G(\xi) = \frac{\bar{\rho}_0}{\bar{b}_0} \frac{A}{\sqrt{1 - \xi^2}}. \quad (E10)$$

Thus, a self-similar solution of the required form does exist. In planar geometry, this is

$$v = \xi, \quad b = \frac{1}{t} \frac{A}{(1 - \xi^2)^{1/2}}, \quad \rho = \frac{F(\xi)}{t}, \quad (\text{E11})$$

and in the spherical geometry

$$v = \xi, \quad b = \frac{1}{t^2} \frac{A}{\xi(1 - \xi^2)^{1/2}}, \quad \rho = \frac{1}{t^3} \frac{F(\xi)}{\xi^2}. \quad (\text{E12})$$

In both cases, the magnetization parameter of fluid elements decreases linearly with time:

$$\sigma = \frac{b^2}{\rho} = \frac{\bar{b}^2}{\bar{\rho}} \propto t^{-1}. \quad (\text{E13})$$

Clearly, this solution is only applicable for  $\xi < 1$ . Moreover, it cannot be simply truncated at some large  $\xi$  and continued with vacuum. Instead, it should terminate at a shock or smoothly transform into a non-self-similar flow. For our simple test problem, this solution cannot become asymptotically valid up to  $\xi = \beta_{\text{max}}$  given by equation (C13) at very late times ( $t \gg t_c$ ), since it cannot simultaneously satisfy the global conservation of energy and rest mass for an initially uniform shell. This implies a limited region of applicability in the tail of the flow, but not at its head.<sup>15</sup> General considerations, however, show that some similar scalings still apply at the head of the flow at late times:  $\sigma \propto t^{-1}$  while  $\rho \propto t^{-1}$  ( $t^{-3}$ ) in planar (spherical) geometry. Moreover,  $v = \xi$  at asymptotic late times when the magnetic pressure becomes dynamically unimportant and each fluid element moves ballistically.

Finally, we calculate the scalings of the total kinetic  $E_{\text{kin}}(t, \xi_1, \xi_2)$  and magnetic  $E_B(t, \xi_1, \xi_2)$  energy of a fluid element bounded by  $x_1 = \xi_1 t$  and  $x_2 = \xi_2 t$ . Both in planar geometry, where  $dV \propto dx = t d\xi$ , and in spherical geometry, where  $dV \propto r^2 dr = t^3 \xi^2 d\xi$ , we obtain

$$E_{\text{kin}}(t, \xi_1, \xi_2) = \int dV \rho \Gamma (\Gamma - 1) \propto t^0, \quad (\text{E14})$$

$$E_B(t, \xi_1, \xi_2) = \int dV \cdot b^2 \left( \Gamma^2 - \frac{1}{2} \right) \propto t^{-1}. \quad (\text{E15})$$

## APPENDIX F: ACCELERATION AFTER THE SEPARATION FROM THE WALL

### F1 Mechanical analogy: two masses and a spring

At  $t < t_0$ , the acceleration of the shell as a whole occurs mainly because the back end of the shell is pushing against the wall, and therefore this mode of acceleration can remain effective only as long as the shell remains in causal contact with the wall. Therefore, the initial shell crossing by the rarefaction wave accelerates the shell up to  $\langle \Gamma \rangle \sim \sigma_0^{1/3}$ , and soon after  $t_0$ , the shell can no longer effectively push against the wall, as the magnetic pressure at the wall drops dramatically, and the subsequent change in the total momentum  $P$  of the shell due to the force  $F$  exerted on it by the wall ( $dP = F dt$ ) becomes negligible.

It is a somewhat surprising result that after the shell separates from the wall, its mean Lorentz factor continues to increase with time, despite the apparent lack of any external force. This can be understood as follows. The total energy and momentum of the shell are indeed conserved in the lack of an external force (or energy losses or gains). However, the shell expands under its own pressure and develops a considerable relative velocity between its leading and trailing edges. In its centre-of-mass frame, the energy and momentum of the front and back ends of the shell are comparable. However, if the expansion is relativistic in the centre of mass (or comoving) frame, then in the laboratory frame, the energy and momentum of the leading part are much larger than those of the trailing part, and thus the leading part dominates the total energy and the Lorentz factor when averaged over the energy in the laboratory frame.

This may be illustrated by the following simple example. Consider two identical masses  $m$  moving together with a compressed ideal massless spring between them, with potential energy,  $E_{\text{pot}}$ , in its own rest frame ( $S_*$ , which is also the rest frame of the two masses, hereinafter the comoving frame). The energy of the system in its own (comoving) rest frame is  $E' = 2mc^2 + E_{\text{pot}}$ , and in a frame where this system is moving at a Lorentz factor  $\Gamma = (1 - \beta^2)^{-1/2}$  in the positive  $x$ -direction (hereinafter, the laboratory frame), its energy is  $E = \Gamma E' = \Gamma(2mc^2 + E_{\text{pot}})$  and its momentum is  $P_x = \Gamma \beta E' / c = \Gamma \beta (2mc^2 + E_{\text{pot}}) / c = \beta E / c$  in the  $x$ -direction (while  $P_y = P_z = 0$ ). The spring is then released and all of its potential energy is converted to kinetic energy of the two masses, which in the comoving frame now move at a Lorentz factor  $\Gamma_* = (1 - \beta_*^2)^{-1/2}$ , such that  $E_{\text{pot}} = 2(\Gamma_* - 1)mc^2$  and  $\Gamma_* = E' / 2mc^2$ , in the positive and negative  $x$ -directions, respectively (the two masses are thus denoted by subscripts ‘+’ and ‘−’ accordingly). In the comoving frame, their energy-momentum four-vectors read  $u_{\pm}^{\mu} = \Gamma_*(1, \pm\beta_*, 0, 0)$ , and a simple Lorentz transformation shows that in the laboratory frame

$$u_{\pm}^{\mu} = [\Gamma \Gamma_* (1 \pm \beta \beta_*), \Gamma \Gamma_* (\beta \pm \beta_*), 0, 0], \quad (\text{F1})$$

which indeed satisfies  $E = E_+ + E_- = mc^2(u_+^0 + u_-^0) = 2\Gamma \Gamma_* mc^2 = \Gamma E'$  and  $P_x = mc(u_+^1 + u_-^1) = \beta E / c$  (and  $P_y = P_z = 0$ ), as it should, while  $\Gamma_{\pm} = E_{\pm} / mc^2 = \Gamma \Gamma_* (1 \pm \beta \beta_*)$ . Thus, the ratios of the energy and momentum of the two masses, and the fractions of the total energy and momentum that each mass holds are given by

$$\frac{E_+}{E_-} = \frac{\Gamma_+}{\Gamma_-} = \frac{1 + \beta \beta_*}{1 - \beta \beta_*}, \quad \frac{P_{x+}}{P_{x-}} = \frac{\Gamma_+ \beta_+}{\Gamma_- \beta_-} = \frac{\beta + \beta_*}{\beta - \beta_*}, \quad \frac{E_{\pm}}{E} = \frac{1 \pm \beta \beta_*}{2}, \quad \frac{P_{x\pm}}{P_x} = \frac{\beta \pm \beta_*}{2\beta}. \quad (\text{F2})$$

<sup>15</sup> Likely, once  $\sigma(\xi_*)$  drops below unity, the flow can no longer efficiently rearrange itself from the original self-similar structure (described in Appendix A) to the new one (described here), as the secondary rarefaction wave becomes weak.

For  $\Gamma, \Gamma_* \gg 1$ , we have

$$\frac{E_-}{E_+} \approx \frac{1}{4} \left( \frac{1}{\Gamma^2} + \frac{1}{\Gamma_*^2} \right) \ll 1, \quad \frac{\Gamma_+}{\Gamma} \approx 2\Gamma_* \gg 1. \quad (\text{F3})$$

Therefore, almost all of the energy in the laboratory frame is in the leading mass (or leading part of the shell), which has greatly increased its Lorentz factor. For  $\Gamma_* = \Gamma$ , the only energy left in the trailing mass (or trailing part of the shell) is its rest-mass energy and all of the potential energy is converted into the kinetic energy of the leading mass, which in this case also carries all of the momentum. Thus, we can see that the leading mass, which constitutes one-half of original rest mass, ends up with almost all of the energy and with a much higher Lorentz factor than what it started with. Going back to our magnetized shell, the potential energy in a ‘spring’ is the analogue of the magnetic energy in the shell, and similarly to the mechanical analogue, eventually, most of the energy ends up in a good fraction of the original rest mass that can reach a very high Lorentz factor (much larger than the initial Lorentz factor of the shell).

## F2 Evolution of $\langle \Gamma \rangle$ after the separation: an alternative derivation of the scaling $\langle \Gamma \rangle \propto t^{1/3}$

Here we follow the mean shell parameters, but drop ‘ $\langle \rangle$ ’ in the notation, for simplicity. Let us consider a planar<sup>16</sup> shell initially (at laboratory frame time  $t = 0$ ) at rest in some rest frame  $S_0$ , which we refer to as the laboratory frame, in which it has a width  $l_0$ , magnetic field  $B_0$ , rest-mass density  $\rho_0$ , magnetization  $\sigma_0 = B_0^2/4\pi\rho_0 c^2 \gg 1$ , energy  $E_0$  and no (or negligible) thermal pressure (for simplicity). This shell can either be leaning against a wall to one end (at  $x = -l_0$ ) or be half of an unbounded shell (initially occupying  $-2l_0 \leq x \leq 0$ ). We have shown that initially the shell expands due to the passage of a self-similar rarefaction wave, which crosses the shell over a time  $t_0 \approx l_0/c$ , and is accelerated to a typical Lorentz factor of  $\Gamma_1 \sim \sigma_0^{1/3}$ .

Now, even though the shell is no longer perfectly uniform as in our initial configuration, we consider the part of the shell that carries most of its energy (as measured in  $S_0$ ), which is expected to be roughly uniform (the relevant physical quantities not changing by more than factors of the order of unity within that region), and make the analogy between it in its own rest frame,  $S_1$  (which moves at a Lorentz factor  $\sim \Gamma_{1,0} \sim \sigma_0^{1/3}$  relative to  $S_0$ ), and our original configuration (that was quantified in  $S_0$ ). Even though this analogy is not perfect, we still expect a similar qualitative behaviour and a similar quantitative behaviour up to factors of the order of unity (which we discard here, as we are interested only in the relevant scaling laws).

One difference, however, is that for reasonably smooth initial conditions, we no longer have a strong rarefaction wave crossing the shell, which eventually splits it into two (as for a perfectly uniform shell with sharp edges surrounded by vacuum on both sides, where the two rarefaction waves from both sides meet and are secondary – our ‘wall’ for a one-sided shell). Thus, the shell is basically the smooth peak of the laboratory frame energy density (which scales as  $B^2$  when  $\sigma \gg 1$ ; see the profile of  $B$  at  $t = 70t_0$  in Fig. 5). The shell still significantly expands in its own rest frame, reaching speeds of the order of its fast-magnetosonic speed on its fast-magnetosonic (or light) crossing time. However, this spreading is smooth and continuous, and the shell does not split into two, but instead it remains a smooth peak of the laboratory frame energy density. Material ahead of the peak in the pressure (at the front of the shell) is accelerated, while material behind this peak (at the back of the shell) is decelerated (by the pressure gradient, in both cases).

None the less, it is instructive to divide this process into discrete steps or phases. The approximate initial conditions of the ‘second phase’ in the evolution of the shell, as expressed in frame  $S_1$  (using a subscript ‘1’ for all the relevant quantities, when measured in this frame), are

$$l_1 \sim \sigma_0^{1/3} l_0, \quad B_1 \sim \frac{B_0}{\sigma_0^{1/3}}, \quad \rho_1 \sim \frac{\rho_0}{\sigma_0^{1/3}}, \quad \sigma_1 \sim \sigma_0^{2/3}, \quad E_1 \sim \frac{E_0}{\sigma_0^{1/3}}.$$

In frame  $S_1$ , the two sides of the shell are expected to accelerate in opposite directions and develop velocities of the order of the shell’s magnetosonic speed,  $\Gamma_{2,1} \sim \sigma_1^{1/3} \sim \sigma_0^{2/9}$ , on the shell’s magnetosonic (or light) crossing time,  $t_1 \sim l_1/c \sim \sigma_0^{1/3} t_0$  (as measured in frame  $S_1$ ). The same scalings as before should approximately hold here as well:

$$l_2 \sim \sigma_1^{1/3} l_1 \sim \sigma_0^{5/9} l_0, \quad B_2 \sim \frac{B_1}{\sigma_1^{1/3}} \sim \frac{B_0}{\sigma_0^{5/9}}, \quad \rho_2 \sim \frac{\rho_1}{\sigma_1^{1/3}} \sim \frac{\rho_0}{\sigma_0^{5/9}}, \quad \sigma_2 \sim \sigma_1^{2/3} \sim \sigma_0^{4/9}, \quad E_2 \sim \frac{E_1}{\sigma_1^{1/3}} \sim \frac{E_0}{\sigma_0^{5/9}}.$$

We note that in frame  $S_0$  (i.e. in the laboratory frame), almost all of the energy ends up in the front part of the shell (which was accelerated in the direction of motion of  $S_1$  relative to  $S_0$ ), whose rest frame  $S_2$  moves at a Lorentz factor  $\Gamma_{2,0} \sim \Gamma_{1,0} \Gamma_{2,1} \sim \sigma_0^{5/9}$  relative to  $S_0$  and has an energy of  $E_{2,0} \sim \Gamma_{2,0} E_2 \sim E_0$  as measured in  $S_0$ . The back part of the shell has a Lorentz factor of  $\sim \Gamma_{1,0} / \Gamma_{2,1} \sim \sigma_0^{1/9}$  in frame  $S_0$ , while its energy in frame  $S_0$  is  $\sim \sigma_0^{1/9} E_2 \sim E_0 / \sigma_0^{4/9}$ , that is, a factor of  $\sim \sigma_0^{4/9} \gg 1$  smaller than that of the forward half of the shell, so it can be safely discarded, as we are interested in the part of the shell that carries most of the energy in frame  $S_0$ . In frame  $S_0$ , the second phase of acceleration takes a time  $t_{1,0} \sim \Gamma_{1,0} t_1 \sim \sigma_0^{2/3} t_0$ . During this time,  $\Gamma$  increased from  $\Gamma_{1,0} \sim \sigma_0^{1/3}$  to  $\Gamma_{2,0} \sim \sigma_0^{5/9}$ , that is, by a factor of  $\sim \sigma_0^{2/9}$ , implying

$$\frac{\Gamma_{2,0}}{\Gamma_{1,0}} \sim \sigma_0^{2/9} \sim \left( \frac{t_{1,0}}{t_0} \right)^{1/3} \implies \Gamma \propto t^{1/3}. \quad (\text{F4})$$

Similarly, recursively repeating the same procedure  $n$  times, it can be shown that

$$U_n \sim \sigma_{n-1}^{1/3} U_{n-1} \sim \sigma_0^{1-(2/3)^n} U_0,$$

<sup>16</sup> The same reasoning essentially holds for a spherical geometry, as demonstrated in Appendix D.

where  $U_n = (l_n, t_n, \Gamma_{n,0}, B_n^{-1}, \rho_n^{-1}, \sigma_n^{-1}, E_n^{-1})$  and  $\Gamma_{0,0} = 1$ . Noting that  $t_{n,0} \sim \Gamma_{n,0} t_n \sim t_n^2/t_0$ , this implies that

$$\frac{\log \sigma_n}{\log \sigma_0} \sim \left(\frac{2}{3}\right)^n, \quad \frac{\log \Gamma_{n,0}}{\log \sigma_0} \sim \left[1 - \left(\frac{2}{3}\right)^n\right], \quad \frac{\log \left(\frac{t_{n-1,0}}{t_0}\right)}{\log \sigma_0} \sim 2 \left[1 - \left(\frac{2}{3}\right)^{n-1}\right], \quad \frac{\log \left(\frac{\Gamma_{n,0}}{\Gamma_{1,0}}\right)}{\log \sigma_0} \sim \frac{2}{3} \left[1 - \left(\frac{2}{3}\right)^{n-1}\right],$$

and

$$\frac{\log(\Gamma_{n,0}/\Gamma_{1,0})}{\log(t_{n-1,0}/t_0)} = \frac{1}{3} \implies \Gamma \propto t^{1/3}. \quad (\text{F5})$$

It can also be seen that in the limit<sup>17</sup> of  $n \gg 1$ ,  $\Gamma_{n,0} \rightarrow \sigma_0$ , that is, the Lorentz factor approaches its asymptotic value that is achieved when  $\sigma \sim 1$  at  $t_c \sim \sigma_0^2 t_0$ . This implies a transition radius to the coasting phase of  $R_c \sim \sigma_0^2 l_0 \sim \Gamma_c^2 l_0$ , where  $\Gamma_c = \Gamma(R_c) \sim \sigma_0$ . Up until this time the shell width in the laboratory frame ( $S_0$ ) remains approximately constant,  $l_{n,0} \sim l_n/\Gamma_{n,0} \sim l_0$ .

This derivation relies on the fact that the shell, which represents the leading part of the flow, carries most of the total energy and rest mass during the impulsive acceleration phase, so that its energy and rest mass are practically constant. As we have seen in Section 2.2, this condition is satisfied for at least as long as the shell remains highly magnetized,  $\sigma \gtrsim 1$ .

## APPENDIX G: THE CM FRAME AND CALCULATIONS IN DIFFERENT FRAMES OF REFERENCE

Let us consider a frame of reference  $S_1$  moving at a dimensionless velocity  $\beta_1$  in the positive  $x$ -direction relative to the laboratory frame and let us denote quantities measured in this frame with a prime. Also, let  $(t_a, x_a) = (t'_a, x'_a) = (0, 0)$  correspond to the event ‘a’ of exposing the original front of the magnetized shell at rest to the vacuum, that is, the onset of motion of the shell material. It is easy to show that the event ‘b’ of the original rarefaction wave hitting the wall corresponds to  $(t_b, x_b) = (t_0, -l_0)$ , where  $t_0 = l_0/c_{\text{ms},0} = l_0[(1 + \sigma_0)/\sigma_0]^{1/2}$  and  $(t'_b, x'_b) = t_0 \Gamma_1 (1 + \beta_1 c_{\text{ms},0}, -\beta_1 - c_{\text{ms},0})$ . Initially (at  $t' = 0$ ), the shell width, density and rest mass are  $l'_0 = l_0/\Gamma_1$ ,  $\rho'_0 = \Gamma_1 \rho_0$  and  $M_0 = \rho_0 l_0 = \rho'_0 l'_0$ , respectively, so that

$$T'^{0x} = -\rho_0(1 + \sigma_0)\Gamma_1 u_1, \quad P'_0 = l'_0 T'^{0x} = -M_0(1 + \sigma_0)u_1. \quad (\text{G1})$$

Now, between  $t' = 0$  and  $t' = t'_b = \Gamma_1(1 + \beta_1 c_{\text{ms},0})l_0[(1 + \sigma_0)/\sigma_0]^{1/2}$ , the momentum increases due to the external force exerted by the wall,  $dP'/dt' = \rho_0 \sigma_0/2$ , so that at  $t' = t'_b$  when the rarefaction wave reaches the wall and the wall is removed (so that from that point onwards there are no external forces, and the total momentum  $P'$  and energy  $E'$  remain constant) we have

$$P'(t' \geq t'_b) = P'_0 + t'_b \frac{\rho_0 \sigma_0}{2} = -M_0(1 + \sigma_0)u_1 + M_0 \Gamma_1 \frac{\sigma_0}{2} \left[ \sqrt{\frac{1 + \sigma_0}{\sigma_0}} + \beta_1 \right]. \quad (\text{G2})$$

We are interested in the CM frame in which by definition  $P' = 0$ . Note that here, in contrast to the previous subsection, we evaluate the total momentum simultaneously in this frame, rather than in the laboratory frame. According to equation (G2), this corresponds to

$$\beta_{\text{CM}} = \frac{\sqrt{\sigma_0(1 + \sigma_0)}}{2 + \sigma_0}, \quad \Gamma_{\text{CM}} = \frac{2 + \sigma_0}{\sqrt{4 + 3\sigma_0}}. \quad (\text{G3})$$

At the CM frame (which moves at  $\beta_1 = \beta_{\text{CM}}$  relative to the laboratory frame),  $P'(t' \geq t'_b) = 0$ , so that the total momentum remains zero from the time when the shell separates from the wall. In this sense, the shell as a whole simply does not accelerate in the CM frame at  $t' \geq t'_b$ . Moreover, the energies of the front part and the back part are comparable in this frame. The total energy at  $t' = 0$  is

$$T'^{00} = \rho_0 \left[ \Gamma_1^2(1 + \sigma_0) - \frac{\sigma_0}{2} \right], \quad E'_0 = l'_0 T'^{00} = M_0 \left[ \Gamma_1(1 + \sigma_0) - \frac{\sigma_0}{2\Gamma_1} \right], \quad (\text{G4})$$

and between  $t' = 0$  and  $t'_b$ , it decreases due to the negative work performed on it by the receding wall at its back,  $dE'/dt' = \mathbf{F} \cdot \mathbf{v} = -\beta_1 \rho_0 \sigma_0/2$ , so that

$$E'(t' \geq t'_b) = E'_0 - t'_b \beta_1 \frac{\rho_0 \sigma_0}{2} = M_0 \left[ \Gamma_1(1 + \sigma_0) - \frac{\sigma_0}{2\Gamma_1} \right] - M_0 \frac{\sigma_0}{2} u_1 \left[ \sqrt{\frac{1 + \sigma_0}{\sigma_0}} + \beta_1 \right] = M_0 \Gamma_1 \left[ 1 + \frac{\sigma_0 - \beta_1 \sqrt{\sigma_0(1 + \sigma_0)}}{2} \right]. \quad (\text{G5})$$

For  $\beta_1 = \beta_{1,\text{CM}}$  given by equation (G3), this reduces to

$$E'_{\text{CM}}(t' \geq t'_b) = \frac{\sqrt{4 + 3\sigma_0}}{2} M_0 = \frac{E_0}{\Gamma_{1,\text{CM}}}. \quad (\text{G6})$$

The self-similar solution describing the original rarefaction wave can be expressed in a rest frame  $S'$  moving at a velocity  $\beta_w$  in the negative  $x$ -direction relative to the laboratory frame (where the wall is at rest), so that in this frame, the wall is moving at a speed  $\beta_w$  in the positive  $x'$ -direction. This implies

$$\xi' = \frac{x'}{t'} = \frac{\xi + \beta_w}{1 + \beta_w \xi}, \quad \xi = \frac{x}{t} = \frac{\xi' - \beta_w}{1 - \beta_w \xi'} \implies \delta_\xi = \frac{\delta_{\xi'}}{\delta_w}, \quad \delta_v = \frac{\delta_{v'}}{\delta_w}, \quad (\text{G7})$$

<sup>17</sup> In practice, the approximation that  $\sigma \gg 1$  breaks down at  $\sigma = \sigma_{\text{min}} \sim$  a few, after  $\approx \log(\log \sigma_{\text{min}}/\log \sigma_0)/\log(2/3)$  steps, or  $\sim 4-6$  for  $\sigma_0 \sim 10^3$  and  $\sigma_{\text{min}} \sim 1.8-3.9$ , so even for  $\sigma_0 \gg 1$ , the shell becomes kinetic-energy-dominated within a rather small number of steps.

$$\delta_{v'} = \delta_{\text{cms},0}^{2/3} \delta_w^{1/3} \delta_{\xi'}^{2/3}, \quad v' = \frac{\delta_{\text{cms},0}^{4/3} \delta_w^{2/3} \delta_{\xi'}^{4/3} - 1}{\delta_{\text{cms},0}^{4/3} \delta_w^{2/3} \delta_{\xi'}^{4/3} + 1}, \quad \Gamma' = \frac{\delta_{\text{cms},0}^{4/3} \delta_w^{2/3} \delta_{\xi'}^{4/3} + 1}{2\delta_{\text{cms},0}^{2/3} \delta_w^{1/3} \delta_{\xi'}^{2/3}}, \quad u' = \Gamma' v' = \frac{\delta_{\text{cms},0}^{4/3} \delta_w^{2/3} \delta_{\xi'}^{4/3} - 1}{2\delta_{\text{cms},0}^{2/3} \delta_w^{1/3} \delta_{\xi'}^{2/3}}, \quad (\text{G8})$$

$$\delta_{\text{cms}} = \frac{\delta_{\text{cms},0}^{2/3} \delta_w^{1/3}}{\delta_{\xi'}^{1/3}}, \quad c_{\text{ms}}^2 = \frac{\sigma}{1 + \sigma} = \left[ \frac{\delta_{\text{cms},0}^{4/3} \delta_w^{2/3} \delta_{\xi'}^{-2/3} - 1}{\delta_{\text{cms},0}^{4/3} \delta_w^{2/3} \delta_{\xi'}^{-2/3} + 1} \right]^2, \quad (\text{G9})$$

$$\frac{\sigma}{\sigma_0} = \frac{\rho}{\rho_0} = \frac{1}{4\sigma_0} \left( \frac{\delta_{\text{cms},0}^{2/3} \delta_w^{1/3}}{\delta_{\xi'}^{1/3}} - \frac{\delta_{\xi'}^{1/3}}{\delta_{\text{cms},0} \delta_w} \right)^2. \quad (\text{G10})$$

Using this result, one can rewrite the integrals in Section C3 in terms of quantities in frame  $S'$ . In particular, they retain the same form up to the following simple substitutions:

$$t \rightarrow t', \quad y \rightarrow y' = \delta_{\xi'}^{2/3}, \quad a \rightarrow a' = \delta_{\text{cms},0}^{2/3} \delta_w^{1/3} \quad y_{\min}(t) \rightarrow y'_{\min}(t') = \delta_{\xi'}^{2/3}. \quad (\text{G11})$$

Finally,  $\xi'_*(t')$  can be computed either by using the solution for  $\xi_*(t)$  and the relation  $\xi'_*(t') = [\xi_*(t) + \beta_w]/[1 + \beta_w \xi_*(t)]$  or by directly generalizing the derivation from Section C2 as follows:

$$\beta'_* = \frac{dx'_*}{dt'} = \frac{v'(\xi'_*) + c_{\text{ms}}(\xi'_*)}{1 + v'(\xi'_*)c_{\text{ms}}(\xi'_*)} = \frac{\delta_{\text{cms},0}^{8/3} \delta_w^{4/3} \delta_{\xi'_*}^{2/3} - 1}{\delta_{\text{cms},0}^{8/3} \delta_w^{4/3} \delta_{\xi'_*}^{2/3} + 1}, \quad \Rightarrow \quad \frac{d\delta_{\xi'_*}^2}{d \ln t'} = \delta_{\xi'_*}^2 + 1 - \frac{(\delta_{\xi'_*}^2 + 1)^2}{\delta_{\text{cms},0}^{8/3} \delta_w^{4/3} (\delta_{\xi'_*}^2)^{1/3} + 1}, \quad (\text{G12})$$

which has the solution

$$\frac{t'}{t'_{0,*}} = \left( \delta_{\xi'_*}^2 + 1 \right) \left[ 1 - \left( \frac{\delta_{\xi'_*}^2}{\delta_{\text{cms},0}^4 \delta_w^2} \right)^{2/3} \right]^{-3/2}, \quad (\text{G13})$$

where  $\delta_w \delta_{\text{cms},0}^{-1} \leq \delta_{\xi'_*} < \delta_w \delta_{\text{cms},0}^2$  and

$$\frac{t'_{0,*}}{t'_0} = \frac{(\delta_{\text{cms},0}^4 - 1)^{3/2}}{\delta_{\text{cms},0}^4 (\delta_{\text{cms},0}^2 + \delta_w^2)}, \quad \frac{t'_{0,*}}{t_0} = \frac{t_{0,*}}{\delta_w t_0} = \frac{(\delta_{\text{cms},0}^4 - 1)^{3/2}}{\delta_w \delta_{\text{cms},0}^4 (\delta_{\text{cms},0}^2 + 1)} = \frac{4\sigma_0^{3/4} (1 + \sigma_0)^{1/4}}{\delta_w (\sqrt{1 + \sigma_0} + \sqrt{\sigma_0})^2}, \quad (\text{G14})$$

where we use the notation  $t'_0 = t'_b$  and the relation

$$\frac{t'_0}{t_0} = \Gamma_w (1 - \beta_w c_{\text{ms},0}) = \frac{(\delta_{\text{cms},0}^2 + \delta_w^2)}{\delta_w (\delta_{\text{cms},0}^2 + 1)}. \quad (\text{G15})$$

For  $\sigma_0 \gg 1$  (and  $\delta_w \ll \delta_{\text{cms},0}$ ), we find that  $t'_{0,*} \approx t'_0$  so that at  $t' \gg t'_0$ , we have  $\delta_{\xi'_*}^2 \approx 2/(1 - \xi'_*) \gg 1$  and

$$\frac{t'}{t'_0} \approx \frac{2}{1 - \xi'_*} \left[ 1 - \frac{1}{4\sigma_0^{4/3} \delta_w^{4/3} (1 - \xi'_*)^{2/3}} \right]^{-3/2}, \quad 1 - \xi'_* \approx \begin{cases} 2t'_0/t' & t' \ll 16\sigma_0^2 \delta_w^2 t'_0, \\ \frac{1}{8\sigma_0^2 \delta_w^2} \left[ 1 + \frac{3}{2} \left( \frac{t'}{16\sigma_0^2 \delta_w^2 t'_0} \right)^{-2/3} \right] & t' \gg 16\sigma_0^2 \delta_w^2 t'_0 \end{cases} \quad (\text{G16})$$

so that  $t'_c/t'_0 \sim \sigma_0^2 \delta_w^2$  or  $t'_c/t'_0 \sim \sigma_0$  for  $\delta_w = \delta_{w,\text{CM}} \sim \sigma_0^{-1/2}$ . Since  $t'_0 \approx t_0/\delta_w$ , this implies  $t'_c \approx \sigma_0^2 \delta_w t_c$ .

It is useful to calculate the ratio of magnetic to kinetic energies:

$$\frac{E'_{\text{EM}}[> \xi'_*(t')]}{E'_{\text{kin}}[> \xi'_*(t')]} = \frac{3}{4} \left( \frac{g[(a')^2] - g[y'_{\min}(t')]}{f[(a')^2] - f[y'_{\min}(t')]} \right), \quad \Rightarrow \quad \frac{E'_{\text{EM}}(t'_0)}{E'_{\text{kin}}(t'_0)} = \frac{3}{4} \left[ \frac{g(\delta_w^{2/3} \delta_{\text{cms},0}^{4/3}) - g(\delta_w^{2/3} \delta_{\text{cms},0}^{-2/3})}{f(\delta_w^{2/3} \delta_{\text{cms},0}^{4/3}) - f(\delta_w^{2/3} \delta_{\text{cms},0}^{-2/3})} \right]. \quad (\text{G17})$$

For the CM frame, we have

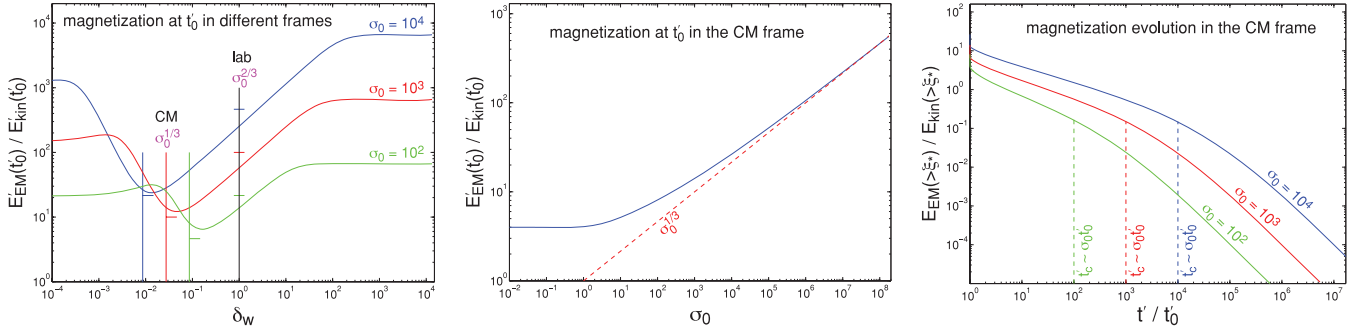
$$\beta_{w,\text{CM}} = -\beta_{\text{CM}} = -\frac{\sqrt{\sigma_0(1 + \sigma_0)}}{2 + \sigma_0}, \quad \delta_{w,\text{CM}}^2 = \frac{2 + \sigma_0 - \sqrt{\sigma_0(1 + \sigma_0)}}{2 + \sigma_0 + \sqrt{\sigma_0(1 + \sigma_0)}} \approx \frac{3}{4\sigma_0} \approx (2\Gamma_{\text{CM}})^{-2} \approx 3\delta_{\text{cms},0}^{-2}. \quad (\text{G18})$$

We also generalize the result for the total energy in the flow:

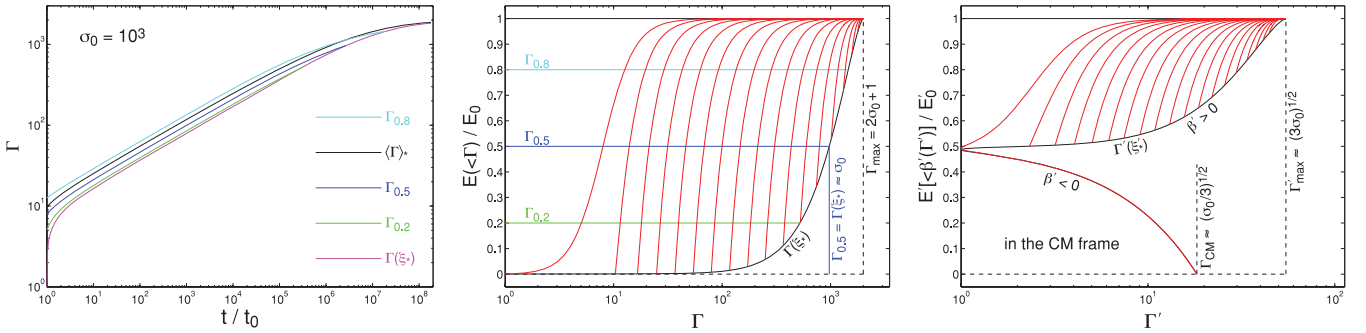
$$\frac{E'(> \xi'_*(t'))}{E'(t'_0)} = \frac{\sqrt{1 + \sigma_0}}{16(2 + \sigma_0)\sigma_0^{3/2}} \left( \frac{t'}{t'_0} \right) \frac{1 - \beta_w \sqrt{\frac{\sigma_0}{1 + \sigma_0}} (a'^2 - y'_{\min})^3 [y'_{\min}(1 + a'^6) + 3a'^2(1 + a'^2 y'_{\min}^2)]}{1 + \beta_w \frac{\sqrt{\sigma_0(1 + \sigma_0)}}{2 + \sigma_0} a'^6 y'_{\min} (y'_{\min}^3 + 1)}, \quad (\text{G19})$$

and the same holds for the energy above some  $\xi' > \xi'_*(t')$ , where  $y'_{\min}(t') = \delta_{\xi'_*}^{2/3}$  is replaced by  $y'(t') = \delta_{\xi'}^{2/3}$ . One can verify that this ratio is indeed 1 at  $t' = t'_0$  when  $y'_{\min} = (\delta_w/\delta_{\text{cms},0})^{2/3} = \delta_w/a'$ .

Fig. G1 shows  $E'_{\text{EM}}/E'_{\text{kin}}$  first at  $t'_0$  as a function of the velocity of the primed frame of reference (left-hand panel), then at  $t'_0$  for the CM frame as a function of  $\sigma_0$  (middle panel) and finally for the CM frame as a function of time  $t'/t'_0$  (right-hand panel).



**Figure G1.** Left-hand panel: the ratio of electromagnetic to kinetic energy in a frame moving at  $\beta_w$  in the negative  $x$ -direction relative to the laboratory frame (i.e. the rest frame of the initial shell and the wall) at time  $t'_0$  when the rarefaction wave reaches the wall, as a function of  $\delta_w$ , for  $\sigma_0 = 10^2, 10^3$  and  $10^4$ . Indicated by vertical lines are the laboratory frame and the CM frame, where this ratio is  $\sim \sigma_0^{2/3}$  and  $\sim \sigma_0^{1/3}$ , respectively (indicated by short horizontal lines). Middle panel: the same for the CM frame as a function of  $\sigma_0$ , using equation (G18); this ratio approaches  $\sigma_0^{1/3}$  (dashed red line) for  $\sigma_0 \gg 1$ . Right-hand panel: the evolution of the same ratio as a function of  $t'/t'_0$  in the CM frame.



**Figure G2.** Left-hand panel: various estimates for the Lorentz factor as a function of time for  $\sigma_0 = 10^3$ ;  $\Gamma_f$  denotes the Lorentz factor below which there is a fraction  $f$  of the total energy. For example,  $\Gamma_{0.5} = \langle \Gamma \rangle_{E, \text{med}}$  is the value for which there is equal energy in faster and slower material. Also shown for reference are  $\Gamma(\xi_*)$  and  $\langle \Gamma \rangle_*$  [which is  $\langle \Gamma \rangle_E$  calculated over the region  $\xi > \xi_*(t)$ ]. Note that  $\Gamma_f$  can be calculated analytically only as long as  $\Gamma_f \geq \Gamma(\xi_*)$ , since otherwise we must include in the calculation the region  $\xi < \xi_*(t)$ , which is not described by the self-similar solution. Middle panel: the corresponding cumulative distribution of the fraction of energy in the flow as a function of  $\Gamma$  for  $\log_{10}(t/t_0) = 0, 0.5, 1, \dots, 8$  (red lines). The lower right-hand boundary (thin solid black curve) corresponds to  $\Gamma(\xi_*)$ . The horizontal blue line corresponds to  $\Gamma_{0.5} = \langle \Gamma \rangle_{E, \text{med}}$  and the vertical blue line shows the value of  $\Gamma$  where it meets with the curve for  $\Gamma(\xi_*)$ :  $\Gamma_{0.5} = \Gamma(\xi_*) \approx \sigma_0$ . Right-hand panel: the corresponding cumulative distribution calculated in the CM frame at  $\log_{10}(t'/t'_0) = 0, 0.25, 0.5, \dots, 4.5$  (red lines). The bottom branch for  $\Gamma'(\xi'_*)$  (thick solid black line) and  $t' = t'_0$  corresponds to material with a negative velocity in the CM frame, which initially carries almost half of the total energy in this frame.

Fig. G2 shows various estimates for the typical Lorentz factor in the laboratory frame as a function of time (left-hand panel), along with the cumulative distribution of energy as a function of the flow Lorentz factor (or velocity) at different times, both in the laboratory frame (middle panel) and in the CM frame (right-hand panel). The first two panels help to quantitatively address an important point that has been raised in Section 4 in the discussion around equations (34) and (35). Taking the energy-weighted average over  $\Gamma$ ,  $\langle \Gamma \rangle_E$ , is not a unique choice and averaging over the four-velocity  $u$ ,  $\langle u \rangle_E$ , would give a similar result. However, as shown in Section 4, using  $\langle \beta \rangle_E$  would give a very different result, where at late times  $\langle \beta \rangle_E \rightarrow \beta_{\text{CM}}$  corresponding to  $\Gamma_{\text{CM}} = (1 - \beta_{\text{CM}}^2)^{-1/2} \sim \sigma_0^{1/2}$ , while  $\langle \Gamma \rangle_E \sim \langle u \rangle_E \sim \sigma_0$ . Fortunately, we can also estimate the typical value of  $\Gamma$  of the material that carries most of the energy in the laboratory frame without having to perform any averaging, thus avoiding the need to choose a specific function of the flow velocity to average over. The left-hand panel of Fig. G2 shows the median value of  $\Gamma$ ,  $\langle \Gamma \rangle_{E, \text{med}} = \Gamma_{0.5}$  (thick solid blue line), according to equation (B5), as well as the values of  $\Gamma$  below, which is a fraction 0.2 ( $\Gamma_{0.2}$ ; green line) or 0.8 ( $\Gamma_{0.8}$ ; cyan line) of the total energy. The middle panel shows the corresponding cumulative distribution of the fraction of the energy in the flow as a function of  $\Gamma$  at different times. Most of the energy in the flow is within a narrow range in  $\Gamma$ , of less than a factor of 2, around  $\langle \Gamma \rangle_{E, \text{med}}$ . Note that  $\langle \Gamma \rangle_{E, \text{med}}$  is also very close to  $\langle \Gamma \rangle_*$ , which is  $\langle \Gamma \rangle_E$  calculated over the region  $\xi > \xi_*$ , and is close to  $\langle \Gamma \rangle_E$  calculated over the whole flow at  $t < t_c = t_0 \sigma_0^2$ . It can be seen that at the time when  $\langle \Gamma \rangle_{E, \text{med}} = \Gamma(\xi_*)$  (after which we can no longer calculate  $\langle \Gamma \rangle_{E, \text{med}}$  semi-analytically), we have  $\langle \Gamma \rangle_{E, \text{med}} = \Gamma(\xi_*) \approx \sigma_0$ , and the Lorentz factor of the plasma in the region  $\xi > \xi_*$  is between  $\approx \sigma_0$  and  $\approx 2\sigma_0$ . Since at that stage most of the magnetic energy is already converted into kinetic energy, as  $\sigma(\xi_*) \sim 0.1$  (see Fig. 3), this should be close to the asymptotic value of  $\langle \Gamma \rangle_{E, \text{med}}$  at late times. Therefore, we can see that all along, from early to late times,  $\langle \Gamma \rangle_{E, \text{med}}$  is very close to  $\langle \Gamma \rangle_E$ . This supports the choice of  $\langle \Gamma \rangle_E$  as being representative of the typical Lorentz factor of the material carrying most of the energy in the laboratory frame.

The right-hand panel of Fig. G2 shows a calculation in the CM frame of the cumulative energy ( $E'$ ) in the flow as a function of its velocity ( $\beta'$ ) or Lorentz factor ( $\Gamma'$ ), and supports the picture described in Section 4 below equation (33). The evolution of the part of the flow ahead of the secondary rarefaction wave ( $\xi' > \xi'_*$ ), which is described by an analytic self-similar solution, is followed from time  $t'_0$  when the original rarefaction wave reaches the wall, and the wall is replaced by vacuum. At  $t' = t'_0$ , this region covers the whole flow and it is easy to see that in the CM frame almost half of the total energy ( $E'_0$ ) is carried by material with a negative velocity ( $\beta' < 0$ ). This is

expected, since by definition, the total momentum vanishes in the CM frame ( $P' = 0$ ) and remains so at later times as well, when a good part of the total energy is at  $\xi' < \xi'_*$ . In the CM frame, we have  $\langle \sigma'(t' = t'_0) \rangle \sim \sigma_0^{1/3}$ , since in the bulk of the flow,  $t'_0$  corresponds to  $t \sim t_0 \sigma_0$  in the laboratory frame and  $\langle \sigma(t = t_0 \sigma_0) \rangle \sim \sigma_0^{1/3}$ . This means that the flow is still highly magnetized at  $t'_0$  and subsequently its front part accelerates while its back side decelerates, as the magnetic energy is transformed into kinetic energy. At  $t'_0 < t' < t'_c \sim t'_0 \sigma_0$ , we have  $\langle \Gamma' \rangle \langle \sigma' \rangle \sim E'_0 / M_0 = E_0 / \Gamma_{\text{CM}} M_0 \sim \sigma_0^{1/2}$  so that the magnetization drops as  $\langle \sigma' \rangle \sim \sigma_0^{1/3} (t' / t'_0)^{-1/3}$ , while the typical Lorentz factor increases as  $\langle \Gamma' \rangle \sim \sigma_0^{1/6} (t' / t'_0)^{1/3}$ . At  $t' = t'_c$ , the combined acceleration at the front and deceleration at the back saturates as the magnetic and kinetic energies become comparable,  $\langle \sigma' \rangle \sim 1$ , and the typical Lorentz factor approaches its asymptotic value,  $\langle \Gamma' \rangle \sim \sigma_0^{1/2}$ . Similar to the laboratory frame, at  $t' > t'_c$ , there is also a coasting phase in the CM frame, where  $\langle \Gamma' \rangle \sim \sigma_0^{1/2}$ , while the magnetization continues to drop as  $\langle \sigma' \rangle \sim t'_0 / t'$ . However, in the CM frame, there is comparable mass and energy in material with  $\Gamma' \sim \sigma_0^{1/2}$  moving in the positive and negative  $x'$ -directions, so that the total momentum adds up to zero.

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